

## Asymmetric barrier model for heavy ion fusion and its relation to channel coupling

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**Abstract.** A new asymmetric parabolic effective fusion barrier model for heavy ion fusion is developed.

**Keywords.** Asymmetric parabolic barrier; heavy ion fusion.

**PACS No.** 25.70.Jj

### 1. Introduction

One expects that coupling effects in the mechanism of heavy ion (HI) fusion may dramatically change the shape of the barrier particularly in the region  $r$  interior to the Coulomb barrier position  $R_B$  such that there is a sharp fall of the potential in the interior region which results in an asymmetric barrier. Based on the exact transmission coefficient across an asymmetric parabolic barrier derived by Zafar Ahmed [1] and the ideas used earlier in our effective fusion barrier transmission model [2] we develop a new asymmetric parabolic effective fusion barrier model for heavy ion fusion. The expected change of shape of the barrier is represented by a variable curvature parameter  $\omega_2$  whereas the outer curvature  $\omega_1$  is kept unchanged.

### 2. Formulation

We explicitly use an asymmetric parabolic type barrier given by the potential

$$V(x) = \left( V_1 - \frac{1}{2} \mu \omega_1^2 x^2 \right) \theta(x) + \left( V_2 - \frac{1}{2} \mu \omega_2^2 x^2 \right) \theta(-x). \quad (1)$$

$\theta(x)$  is a step function such that  $\theta(x) = 1, x > 0$  and  $\theta(x) = 0, x \leq 0$ .  $V_i$  and  $\omega_i, i = 1, 2$  indicate the height and the curvature factors, respectively, and  $\mu$  stands for the reduced mass. The potential barrier can be used to simulate the Coulomb barrier for any partial wave in the neighborhood of  $R_B$  which is taken to be at the origin in this particular expression (1). In a fusion calculation we set  $V_1 = V_2 = V_B$ .

By defining  $\alpha_i = (V_B - E_{cm})/\hbar\omega_i, i = 1, 2$  and an asymmetric parameter  $\eta = \sqrt{\omega_2/\omega_1}$  the transmission coefficient [1] at center of mass energy  $E_{cm}$  is given as

$$T(E_{cm}) = \frac{1}{\frac{1}{4}\sqrt{1 + e^{2\pi\alpha_1}}\sqrt{1 + e^{2\pi\alpha_2}} \left[ \eta \left( \frac{f_1}{f_2} \right) + \frac{1}{\eta} \left( \frac{f_2}{f_1} \right) \right] + \frac{1}{2} [e^{\pi\alpha_1} e^{\pi\alpha_2} + 1]}, \quad (2)$$

where  $f_1 = f(\alpha_1)$  and  $f_2 = f(\alpha_2)$ . The function  $f(\alpha) = \left| \Gamma \left( \frac{1}{4} + i\frac{\alpha}{2} \right) / \Gamma \left( \frac{3}{4} + i\frac{\alpha}{2} \right) \right|$ , can be approximated by  $f_{approx}(\alpha) = 1/\sqrt{\gamma}(1 + 1/8\gamma)$ , where  $\gamma = \sqrt{(1/16) + (\alpha^2/4)}$ .

In order to consider the Coulomb barriers generated by different partial waves  $l$ , we need to replace the height  $V_B$  of the effective barrier by

$$V_B^l = V_B + \frac{\hbar^2}{2\mu} \frac{l(l+1)}{R_B^2}.$$

The quantities  $V_B, R_B$  and the outer region ( $r > R_B$ ) curvature factor  $\omega_1$  can be obtained using the following global formulae:

$$R_B = r_0 \left( A_1^{1/3} + A_2^{1/3} \right) + 2.72 \text{ fm}, \quad V_B = \frac{Z_1 Z_2 e^2}{R_B} \left( 1 - \frac{a}{R_B} \right)$$

and

$$(\hbar\omega_1)^2 = \frac{Z_1 Z_2 e^2 \hbar^2}{\mu R_B^2} \left( \frac{1}{a} - \frac{2}{R_B} \right),$$

where  $a = 0.63$  fm and  $r_0 = 1.07$  fm,  $A_j, Z_j, j = 1, 2$  denote the mass number and proton number of the two colliding nuclei, respectively. We control the inner region ( $r < R_B$ ) curvature factor  $\omega_2$  by varying the parameter  $\eta = \sqrt{\omega_2/\omega_1}$ .

Using the above specifications we adopt the expression (2) to calculate transmission coefficient  $T_l(E_{cm})$  for different  $l$ 's as a function of incident energy. This is then used to obtain the results for  $\sigma_F^l, \sigma_F, \langle l \rangle$  and  $D(E_{cm})$  given by the formulae:

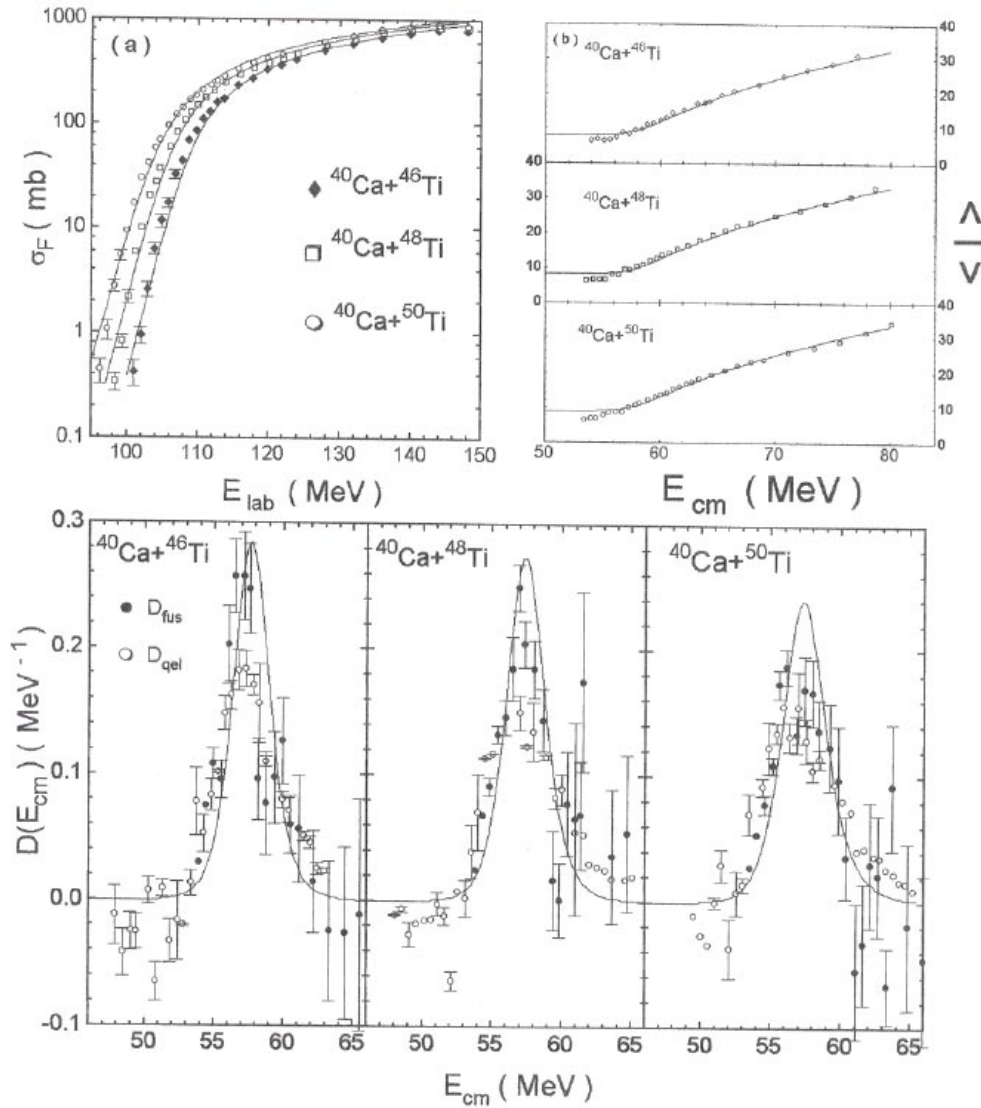
$$\sigma_F^l = \frac{\pi}{k^2} (2l+1) T_l, \quad \sigma_F = \sum_{l=0}^{\infty} \sigma_F^l,$$

$$\langle l \rangle = \frac{\sum_{l=0}^{\infty} l \sigma_F^l}{\sigma_F} \quad \text{and} \quad D(E_{cm}) = \frac{d^2(E\sigma_F)}{dE^2},$$

where  $k = \sqrt{(2\mu/\hbar^2)E_{cm}}$ .

### 3. Results and discussion

In figure 1(a) and (b) (upper panel) we show by solid curve the variation of  $\sigma_F$  and  $\langle l \rangle$ , respectively, with energy for  $^{40}\text{Ca} + ^{46,48,50}\text{Ti}$  systems.  $E_{lab}$  indicates energy in the laboratory frame. From these figures it is clear that fit to the experimental data is good. Values



**Figure 1.** Upper panel shows the variation of (a)  $\sigma_F$  and (b)  $\langle l \rangle$  with energy for  $^{40}\text{Ca} + ^{46,48,50}\text{Ti}$  systems. Lower panel shows the variation of  $D(E_{cm})$  with  $E_{cm}$ . Solid curves represent the results of present calculation. The experimental data are taken from ref. [4].

of  $V_B$ ,  $R_B$ ,  $\hbar\omega_1$  and  $\eta$  used in the calculation for these systems are listed in table 1. In the lower panel of figure 1, we show the results for  $D(E_{cm})$  obtained by using point-difference formula used in ref. [3] for the  $^{40}\text{Ca} + ^{46,48,50}\text{Ti}$  systems. The fit to the experimental data in these cases is impressive. If one examines  $D$ , the  $D$  variation curve becomes broader and shorter in height for larger  $\eta$  as in the case of  $^{40}\text{Ca} + ^{50}\text{Ti}$  system (see table 1) where more channels are involved.

**Table 1.** Systems and  $s$ -wave barrier radius  $R_B$ , its height  $V_B$ , curvature factor  $\hbar\omega_1$  and the asymmetry parameter  $\eta$ .

System	$R_B$ (fm)	$V_B$ (MeV)	$\hbar\omega_1$ (MeV)	$\eta$
$^{40}\text{Ca} + ^{46}\text{Ti}$	10.32	57.65	4.02	1.4
$^{40}\text{Ca} + ^{48}\text{Ti}$	10.37	57.36	3.96	1.5
$^{40}\text{Ca} + ^{50}\text{Ti}$	10.39	57.76	3.91	1.8

### Acknowledgement

BS acknowledges support (Grant No.SP/S2/K14/96(PRU)) from DST, New Delhi and the facilities extended by North-Eastern Hill University, Shillong and Institute of Physics, Bhubaneswar.

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