

## Effective collision strengths among the fifteen lowest states of FeXVII

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**Abstract.** Collision strengths have been calculated for electron impact excitation of neon-like Fe XVII for all transitions within its 15 lowest states. Configuration interaction wavefunctions have been used to represent the target states. The standard *R*-matrix code has been used to calculate the contribution from the lower scattering partial waves ( $L \leq 9$ ), while the no exchange version of the same code has been used to compute efficiently the contribution of higher partial waves ( $L \geq 10$ ). Effective collision strengths for all the 105 transitions are tabulated for elected temperatures in the range  $\log T_e = 5.40$  to  $\log T_e = 7.00$  with  $T_e$  expressed in °K.

**Keywords.** Collision strength; R-matrix method.

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### 1. Introduction

There has been much interest in the study of interaction of electrons and photons with ionized atoms, particularly with metallic impurities such as Ti, Cr, Fe and Ni due to their importance in fusion plasmas [1]. Data on these processes are also required in astrophysics ([2], [3]) and laser research, especially in the soft X-ray region where Ne-like ions play a specific role in the electron excitation scheme, as illustrated in the recent work of Matthew *et al* [4].

The first identification of resonance lines of Fe XVII was made by Tyren [5] in the 12–17 Å region for the transitions arising from  $2p^5 3s$ ,  $2p^5 3d$ ,  $2p^5 4d$  and  $2s 2p^6 3p$  configurations. New laboratory observations in the regions 10–17 Å were reported by Gordon *et al* [6], who identified resonance transitions from  $2p^5 4s$ ,  $2p^5 4d$ ,  $2p^5 5d$ ,  $2p^5 6d$ , and  $2s 2p^6 4p$ . From solar coronal observations Hutcheon *et al* [7] identified resonance lines from  $2p^5 5s$ ,  $6s$ ,  $7s$ ,  $5p$  and  $8d$  and obtained a value of  $1262.2 \pm 1.0$  eV for the ionization energy.

Several authors have reported atomic data for Ne-like ions. Bhatia *et al* [10] have used the distorted-wave (DW) approximation to calculate the collision-strengths at one energy point, for transitions from the ground level to  $n = 3$  Rydberg levels of Ne-like ions with nuclear charge  $Z = 14, 18, 22, 26, 32$  and  $36$ . Mann [8] has used distorted wave method to obtain collision strengths for iron ions in LS coupling. These results have been used by Smith *et al* [9] for obtaining the population rates for individual *J*-levels in Fe XVII where contribution of cascades from higher levels and resonance excitation to each level are also included. Recently Zhang *et al* [11] and Hagelstein *et al* [12] have also reported collision strengths for several Ne-like ions using the relativistic-distorted wave method. All these calculations reported collision strengths at and above the excitation thresholds.

In the present work, we have used the  $R$ -matrix method [13], used successfully by various authors [14]. This allows us to include explicitly the effect of resonances which play an important role and do not appear in the earlier DW calculations. These resonances converge to all the target states which are included in the calculations. We have performed a 15-state  $2s^2 2p^6 ({}^1S^e)$ ,  $2s^2 2p^5 3s ({}^{1,3}P^0)$ ,  $2s^2 2p^5 3p ({}^{1,3}S^e, {}^{1,3}P^e, {}^{1,3}D^e)$ ,  $2s^2 2p^5 3d ({}^{1,3}P^0, {}^{1,3}D^0, {}^{1,3}F^0)$  calculation in which the states are represented by configuration-interaction (CI) wavefunctions. The effective collision strengths, obtained by averaging the collision strengths over a Maxwellian distribution for the velocity of the incident electron, are tabulated over a wide range of temperatures.

We have used the standard  $R$ -matrix code of Berrington *et al* [15, 16] for the low partial wave ( $L \leq 9$ ) and the no-exchange  $R$ -matrix program recently developed by Burke *et al* [17] for partial waves  $10 \leq L \leq 40$ . In addition, for optically allowed transitions, a 'top-up' procedure based on the sum rule of Burgess *et al* [18] has been used to account approximately for  $L > 40$ .

## 2. Target calculations

Using the general CI code CIV3 [19], Hibbert *et al* [20] have calculated CI wave-functions of all the states of the form  $[1s^2] 2s^2 2p^6, 2s^2 2p^5 3l, 2s 2p^6 3l$  ( $l = s, p, d$ ) for many ions of the neon isoelectronic sequence, including Fe XVII. In the present scattering calculation, the fifteen lowest ionic states belonging to the ground  $2s^2 2p^6$  and the  $n = 3$  R  $2s^2 2p^5 3l$  ( $l = s, p, d$ ) configurations are represented by restricted CI expansions, which include the most important configurations while keeping the scattering calculation tractable.

The wavefunctions are represented by an expansion of the form

$$\Psi(LS) = \sum_{i=1}^M a_i \phi_i(\alpha_i LS) \quad (1)$$

where the single configuration function  $\phi_i$  is constructed from one electron orbitals, whose angular momenta are coupled as specified by  $\alpha_i$  to form total  $L$  and  $S$  common to the  $M$  configurations. The radial part of each orbital is written as a linear combination of normalized Slater-type orbitals:

$$P_{nl} = \sum_{i=1}^k b_i \left[ \frac{(2\zeta_i)^{2p_i+1}}{(2p_i)!} \right]^{1/2} r^{p_i} \exp(-\zeta_i r) \quad (2)$$

The parameters  $b_i$  and  $\zeta_i$  in (2) and the mixing coefficients  $\alpha_i$  in (1) are determined variationally as described by Hibbert *et al* [20].

In order to represent in a balanced way the ground and all the  $n = 3$  R states, we used eight orthogonal one-electron orbitals  $1s, 2s, 3s, 3p, 4p, 3d$  and  $4d$ . The  $1s, 2s$  and  $2p$  orbitals were initially chosen as the Hartree-Fock orbitals for the ground  $2P^0$  state of the fluorine-like Fe XVIII ion [21], with the  $1s$  and  $2s$  functions kept frozen throughout the calculation. The  $3s$  function was first optimized on the energy of the lowest  $2p^5 3s {}^3P^0$  Rydberg state of Fe XVII. The  $2p$  was then reoptimized on the same state. Since the new  $2p$  function is not the best one to represent the  $2s^2 2p^6 {}^1S^e$  ground state, we introduced a  $3p$  function to compensate for this, optimizing its parameters by minimizing the lowest energy eigenvalue in the  $(2s^2 2p^6 + 2s^2 2p^5 3p) {}^1S^e$  subspace. This  $3p$  function then provided some flexibility to represent the ' $2p$ '

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orbitals optimal for the different target states. The  $4p$  orbital was optimized on the lowest eigenvalue in the  $(2p^5 3p + 2p^5 4p) {}^3S^e$  subspace. The  $3d$  function was chosen to optimize the lowest energy eigenvalue arising from the configuration  $(2s^2 2p^5 3s + 2s 3d 2p^5 3s) {}^3P^0$ , in order to account for the important  $s - d$  angular correlation. Finally, the  $4d$  orbital was optimized by minimizing the lowest eigenvalue in the subspace  $(2p^5 3d + 2p^5 4d) {}^3D^0$ .

Table 1 lists the optimized parameters  $b_i$ ,  $p_i$  and  $\zeta_i$  for the  $3s$ ,  $2p$ ,  $3p$ ,  $4p$ ,  $3d$  and  $4d$  orbitals. Table 2 gives the restricted list of configurations included in the scattering calculation to represent the 15 target states, which are indexed in the order of increasing energy. Table 3 shows that the excitation thresholds, calculated with these fairly simple wavefunctions, agree reasonably well with the experimental results of Corliss and Sugar [22]

**Table 1.** Value of Parameters  $b_i$ ,  $p_i$ , and  $\zeta_i$  for bound orbitals of Fe XVII.

Orbital	Clementi coefficient $b_i$	Power of $r$ $P_i$	Exponent $\zeta_i$
$3s$	0.22133	1	19.36686
	-1.05835	2	8.35550
	1.54150	3	6.25763
$2p$	0.67008	2	10.56569
	0.14765	2	16.31110
	0.19773	2	9.50033
	0.00222	2	33.58497
$3p$	2.28634	2	9.19396
	-2.66353	3	9.55422
$4p$	1.84875	2	9.28200
	-3.17109	3	9.27711
$3d$	1.96310	4	7.02789
	1.00000	3	12.10647
$4d$	0.60994	3	12.97180
	-1.13602	4	7.04955

**Table 2.** Configurations used in the CI expansion of Fe XVII target state.

Target states	State number	Configurations used
${}^1S^e$	1, 9	$[1s^2] 2s^2 2p^6, 2s^2 2p^5 3p, 2s^2 2p^5 4p, 2s 2p^6 3s$
${}^3P^0$	2, 10	$[1s^2] 2s^2 2p^5 3s, 2s^2 2p^5 3d, 2s^2 2p^5 4d, 2s 2p^6 3p, 2s 2p^6 4p$
${}^1P^0$	3, 15	$[1s^2] 2s^2 2p^5 3s, 2s^2 2p^5 3d, 2s^2 2p^5 4d, 2s 2p^6 3p, 2s 2p^6 4p$
${}^3S^e$	4	$[1s^2] 2s^2 2p^5 3p, 2s^2 2p^5 4p, 2s 2p^6 3s$
${}^3D^e$	5	$[1s^2] 2s^2 2p^5 3p, 2s^2 2p^5 4p, 2s 2p^6 3d, 2s 2p^6 4d$
${}^1D^e$	6	$[1s^2] 2s^2 2p^5 3p, 2s^2 2p^5 4p, 2s 2p^6 3d, 2s 2p^6 4d$
${}^3F^e$	8	$[1s^2] 2s^2 2p^5 3p, 2s^2 2p^5 4p$
${}^1P^e$	7	$[1s^2] 2s^2 2p^5 3p, 2s^2 2p^5 4p$
${}^3F^0$	11	$[1s^2] 2s^2 2p^5 3d, 2s^2 2p^5 4d$
${}^1F^0$	12	$[1s^2] 2s^2 2p^5 3d, 2s^2 2p^5 4d$
${}^3D^0$	14	$[1s^2] 2s^2 2p^5 3d, 2s^2 2p^5 4d$
${}^1D^0$	13	$[1s^2] 2s^2 2p^5 3d, 2s^2 2p^5 4d$

**Table 3.** Excitation thresholds for Fe XVII (in R).

Key	Configuration	State	Theory	Experiment
1.	$1s^2 2s^2 2p^6$	$^1S^e$	0-00000	0-00000
2.	$1s^2 2s^2 2p^5 3s$	$^3P^0$	53-58536	53-35012
3.	$1s^2 2s^2 2p^5 3s$	$^1P^0$	53-81748	54-31601
4.	$1s^2 2s^2 2p^5 3p$	$^3S^e$	55-52232	
5.	$1s^2 2s^2 2p^5 3p$	$^3D^e$	55-94257	
6.	$1s^2 2s^2 2p^5 3p$	$^1D^e$	56-13292	
7.	$1s^2 2s^2 2p^5 3p$	$^1P^e$	56-17428	
8.	$1s^2 2s^2 2p^5 3p$	$^3P^e$	56-17428	
9.	$1s^2 2s^2 2p^5 3p$	$^1S^e$	57-70577	
10.	$1s^2 2s^2 2p^5 3d$	$^3P^0$	58-92013	58-98169
11.	$1s^2 2s^2 2p^5 3d$	$^3F^0$	59-12324	
12.	$1s^2 2s^2 2p^5 3d$	$^1F^0$	59-34388	
13.	$1s^2 2s^2 2p^5 3d$	$^1D^0$	59-42062	
14.	$1s^2 2s^2 2p^5 3d$	$^3D^0$	59-42062	59-70797
15.	$1s^2 2s^2 2p^5 3d$	$^1P^0$	60-25818	60-69031

### 3. Scattering calculation

In an inner region  $r < a$  containing the charge distribution of the  $N$ -electron target, the total wavefunction describing the  $(N + 1)$  electron system is expanded on a discrete basis of  $R$ -matrix states [13, 22].

$$\Psi_k = A \sum_{ij} C_{ijk} \phi_i(x_1, x_2 \dots x_n \hat{y}_{n+1} \sigma_{n+1}) U_{ij}(y_{n+1}) + \sum_j d_{jk} \phi_j(x \dots x_{n+1}) \quad (3)$$

where  $A$  is the antisymmetrisation operator which accounts for electron exchange,  $\phi_i$  are channel functions formed by coupling the target states of coordinates  $x_i = (r_i, \hat{r}_i, \sigma_i)$  with the spin angle function of the scattered electron. The  $[u_{ij}]$  form a discrete  $R$ -matrix basis of continuum orbitals for the scattered electron and the  $[\phi_j]$  are  $(N + 1)$  electron bound configurations, which account for the orthogonality of the continuum orbitals  $u_{ij}$  to the bound orbitals and for additional short range correlation effects.

The continuum orbitals  $u_{ij}$  (3) are solutions of the zero-order radial differential equation:

$$\left[ \frac{d^2}{dr^2} + \frac{l_i(l_i + 1)}{r^2} + 2V(r) - K_i^{2j} u_{ij}(r) = \sum \lambda_{ijk} P_k(r) \right] \quad (4)$$

which satisfy the boundary conditions:

$$u_{ij}(0) = 0$$

$$\frac{a}{u_{ij}} \frac{du_{ij}}{dr} \Big|_{r=a} = b \quad (5)$$

in (4),  $l_i$  is the angular momentum of the scattered electron,  $V(r)$  is the static potential of the target in its ground state and  $\lambda_{ijk}$  are Lagrange multipliers which are determined

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in order to ensure the orthogonality of the continuum orbitals to the bound radial orbitals  $P_{kl}(r)$  having the same angular momentum  $l_i$ . We imposed a zero logarithmic derivative  $b = 0$  at the  $R$ -matrix boundary radius  $a = 3.5$  a.u. and we retained 20 continuum orbitals for each angular symmetry, to ensure convergence in the energy range considered here, namely up to 170 R.

The coefficients  $c_{ijk}$  and  $d_{jk}$  in (3) were determined by diagonalizing the  $(N + 1)$ -electron Hamiltonian matrix in the inner region. In the outer region ( $r \geq a$ ), the radial equations were solved, using the asymptotic code of Berrington *et al* [23] which treats multipole couplings by first order perturbation theory [24]. The LS coupled  $K$  matrices, obtained by matching the inner and outer solutions at the  $R$ -matrix boundary were used to calculate collision strengths. We have considered all partial waves up to  $L = 9$  for both parties and both spin multiplicities (doublet and quartet). This was sufficient to obtain converged results for forbidden transitions from the ground state  $1S^e$ . However, for dipole allowed transitions, such as  $2p^6 1S^e \rightarrow 3s 1P^0$ , it was necessary to include the contribution of higher partial waves for convergence. Since exchange effects were found to be negligible for  $L \geq 10$ , a no-exchange  $R$ -matrix approximation, which amounts to neglecting the antisymmetrization and the bound type part of expansion (3), is sufficient for higher partial waves. A fast no-exchange  $R$ -matrix code, recently developed by Burke *et al* [17], has therefore been used to calculate the contribution from  $L = 10$  to 40 and, finally, a 'top up' procedure, based on the sum rule of Burgess *et al* [18], accounts approximately for  $L > 40$ .

Another important aspect of the calculation is that, above all thresholds, the pseudo-resonances, induced in the low partial waves by some bound-type terms in expansion (3), have been removed by smoothing the  $T$ -matrix according to the method of Burke *et al* [24].

## 4. Results and discussion

Figure 1 illustrates the results for excitation from the ground state  $1s^2 2s^2 2p^6 1S^e$  to the first excited state  $1s^2 2s^2 2p^5 3s 3P^0$ . It clearly shows that at low energies, the collision strengths are dominated by closed channel (or Feshbach) resonances. These resonances, which converge towards the Rydberg state thresholds of the  $2s^2 2p^5 (3s, 2p, 3d)$  configurations, are superimposed on a smoothly increasing background.

In table 4 we list our collision strengths  $[\Omega]$  for 105 transitions involving 15 lowest states from 74 to 140 R. Ours are the first close-coupling results for collision-strengths for transitions among the excited states. For transitions from ground-state, calculation has been performed using the DW method by Mann [8] and used by Smith *et al* [9] for the calculation of population rates of various levels. They include radiative cascade from higher excited states and resonance excitation which involves dielectronic capture of free electrons by  $N$ -electron system to form a doubly excited configuration of  $(N + 1)$  electron system. DW method is just a two-state calculation and lacks completely interchannel coupling and fails to predict the collision strengths below the excitation thresholds. Whereas the  $R$ -matrix method is a powerful technique and shows the Feshbach resonances due to autoionized states as shown in figure 1 where  $\Omega$  is plotted for  $2p^6 1S^e \rightarrow 2p^5 3s^3 P^0$  transition. DW method is a high energy approximation therefore Mann [8] has given the results for  $\Delta n = 1$  transition at 2/ energies spaced logarithmically between threshold and 100 time threshold. As the results of Mann [8] are not at regular energy intervals, the exact comparison is

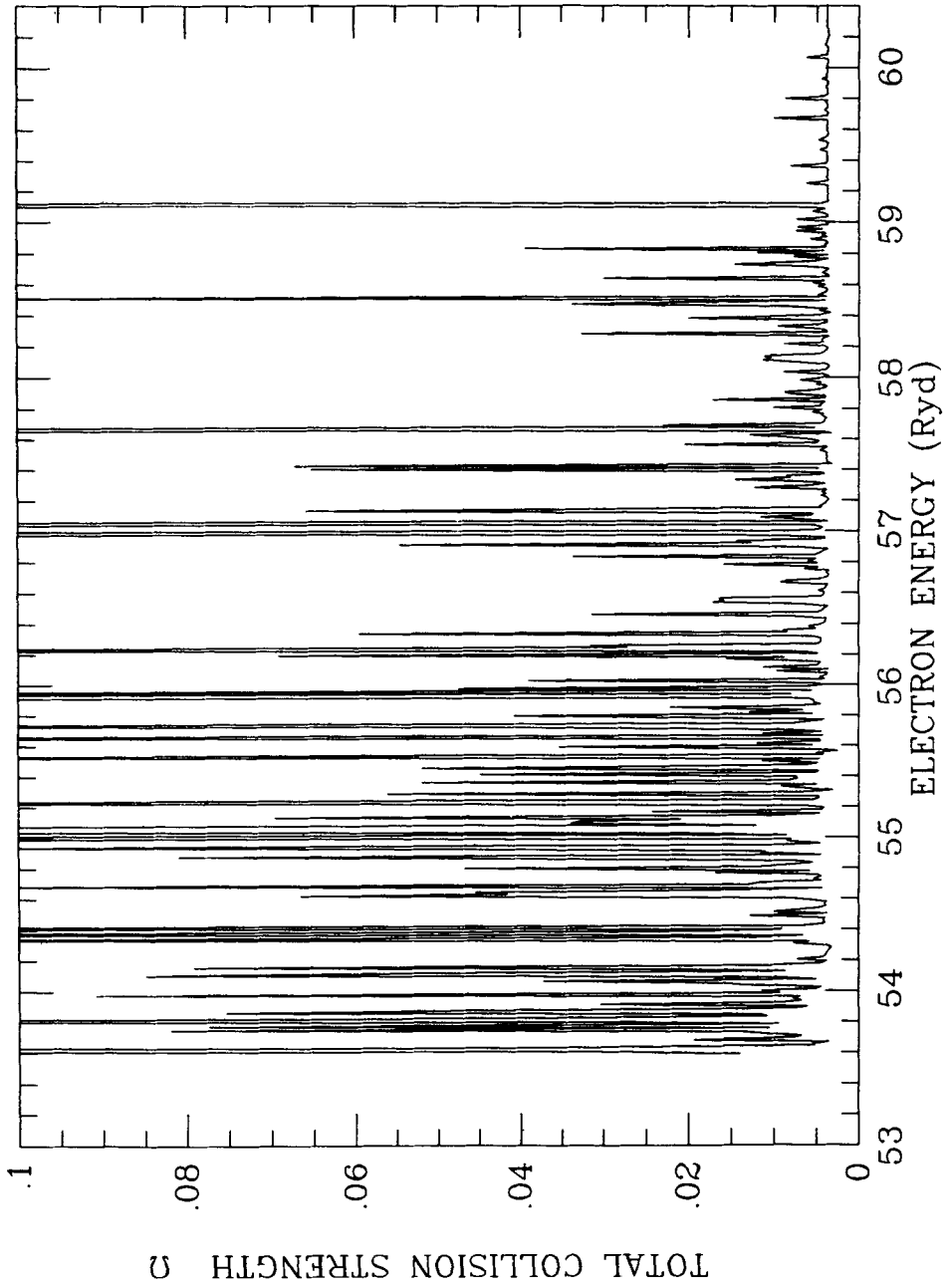


Figure 1.

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difficult. On comparing the results for first forbidden transition  $2p^6 1s^e \rightarrow 2p^5 3s^3 P^0$  we find Mann's results vary from  $\Omega = 8.465 \times 10^{-3}$  at  $E_i = 71.53 \text{ R}$  to  $\Omega = 7.572 \times 10^{-3}$  at  $E_i = 142.48$  which lie quite above our results which are shown in the first row of table 4 where  $\Omega = 8.666 \times 10^{-3}$  at  $E_i = 74.00 \text{ R}$  to  $\Omega = 1.278 \times 10^{-3}$  at  $E_i = 140.00 \text{ R}$ . Clearly the DW result obtained by Mann does not have the correct asymptotic behaviour. This difference may be attributed to physical effects such as interchannel coupling and correlation effects which we have included in our  $R$ -matrix calculations. Recently Zhang *et al* [11] and Hagelstein *et al* [12] have also repeated the calculations for neon-like ions using relativistic-distorted-wave method, but their theories also do not predict the results below the thresholds.

Among the transitions from the ground state we find the collision strengths are maximum for  $2p^6 1s^e \rightarrow 2p^5 3d^1 D$  transition, as obtained by Mann [8] and Zhang *et al* [12]. This is an allowed transition and corresponds to promotion of  $2p$  electron to  $3d$  electron. The energy separation for this transition obtained by Mann is 59.593 R, while for our configuration using interaction technique with limited configuration is 60.258 which is quite near to the experimental result 60.690, as shown in table 3. For this transition the collision strength obtained by Mann varies from  $1.08 \times 10^{-1}$  at 75.742 R to  $\Omega = 1.56 \times 10^{-1}$  at  $E = 140.00 \text{ R}$ . Both these results lie quite below our results as shown in the row corresponding to 1-15 transition in table 4, where  $\Omega$  is  $2.066 \times 10^{-1}$  at  $E = 140 \text{ R}$ . This behaviour may be due to our consistent approach for taking contributions of higher partial waves i.e.  $L \geq 9$  by using no-exchange code recently developed by Burke *et al* [17].

Since the excitation collision strengths vary rapidly with energy in the threshold region, it is not practicable to tabulate them. However, for many plasma applications, excitation rate coefficients rather than the collision strengths are needed. They are obtained by integrating the collision strengths over a Maxwellian distribution of incident electron energies. This is the usual distribution of electron velocities for astrophysical applications but any other distribution can be examined using our  $\Omega$  tabulated in table 4. The excitation rate coefficient [25] for a transition  $i$  to  $f$  at an electron temperature  $T_e$  is given by:

$$C(i \rightarrow f) = \frac{8.63 \times 10^{-6}}{g_i T_e^{1/2}} \gamma(i \rightarrow f) \exp\left[\frac{-\Delta E_{if}}{k T_e}\right] \text{cm}^3 \text{s}^{-1} \quad (7)$$

where  $g_i = (2L_i + 1)(2S_i + 1)$  is the statistical weight of the lower state  $i$ ,  $\Delta E_{if} = E_f - E_i$  is the excitation energy and  $\gamma(i \rightarrow f)$ , defined as:

$$\gamma(i \rightarrow f) = \int_0^{-\infty} \Omega(i \rightarrow f) \exp(-E_f/T_e) d(E_f/T_e) \quad (8)$$

is the effective (dimensionless) collision strength for the transition  $i$  to  $f$ ,  $E_f$  is the energy of the incident electron with reference to upper level  $f$  and  $k$  is the Boltzmann constant.

In table 5, we have given  $\gamma(i \rightarrow f)$  for all the 105 transitions over the electron temperature range from  $\log(T_e) = 5.4$  to  $\log(T_e) = 7.0$  where  $T_e$  is in  $^\circ\text{K}$ .

In general, the value of the effective collision strengths  $\gamma$  are large for dipole allowed transitions (e.g.  $2p^6 1S^e \rightarrow 2p^5 3s^1 P^0$ ) as compared to spin forbidden transitions. Among the  $2p^6 1S^e \rightarrow 2p^5 3p$  transitions, the value of  $\gamma$  is largest for  $2p^6 1S^e \rightarrow 2p^5 3p^1 S^e$ , as obtained by other authors [8, 11, 12]. For  $2p^6 1S^e \rightarrow 2p^5 3d$  transitions, the largest  $\gamma$  was found for the dipole allowed transition  $2p^6 1S^e \rightarrow 2p^5 3d^1 P^0$ . On comparing our

Table 4. Collision strengths for transitions in FE XVII in the energy range 74–140 R. ( $a \pm b \equiv a \times 10^{\pm b}$ )

Transition <i>I</i>	<i>J</i>	Energy (R)														
		74-00	78-00	82-00	85-00	90-00	95-00	110-00	120-00	130-00	140-00					
1	2	8.666	-03 6.344	-03 4.725	-03 3.883	-03 3.022	-03 2.639	-03 2.615	-03 2.449	-03 1.861	-03 1.278	-03				
1	3	6.791	-02 4.265	-02 2.556	-02 1.705	-02 9.166	-03 6.866	-03 1.313	-02 1.559	-02 1.296	-02 9.893	-03				
1	4	3.657	-03 3.436	-03 3.265	-03 3.164	-03 3.034	-03 2.941	-03 2.777	-03 2.711	-03 2.686	-03 2.762	-03				
1	5	8.356	-03 7.492	-03 6.771	-03 6.313	-03 5.684	-03 5.199	-03 4.406	-03 4.320	-03 4.590	-03 5.321	-03				
1	6	5.589	-03 5.528	-03 5.544	-03 5.597	-03 5.745	-03 5.948	-03 6.676	-03 7.114	-03 7.441	-03 7.662	-03				
1	7	2.984	-03 2.785	-03 2.615	-03 2.504	-03 2.345	-03 2.213	-03 1.934	-03 1.826	-03 1.789	-03 1.857	-03				
1	8	1.413	-03 1.230	-03 1.083	-03 9.943	-04 8.789	-04 7.968	-04 6.796	-04 6.662	-04 6.936	-04 7.800	-04				
1	9	3.943	-02 3.893	-02 3.867	-02 3.861	-02 3.874	-02 3.915	-02 4.179	-02 4.470	-02 4.867	-02 5.394	-02				
1	10	1.614	-02 1.513	-02 1.419	-02 1.353	-02 1.249	-02 1.150	-02 8.812	-03 7.232	-03 5.936	-03 5.128	-03				
1	11	1.436	-02 1.324	-02 1.224	-02 1.155	-02 1.050	-02 9.562	-03 7.222	-03 6.023	-03 5.186	-03 4.888	-03				
1	12	4.214	-03 4.245	-03 4.320	-03 4.401	-03 4.569	-03 4.766	-03 5.404	-03 5.785	-03 6.092	-03 6.333	-03				
1	13	5.652	-03 5.176	-03 4.752	-03 4.462	-03 4.024	-03 3.633	-03 2.649	-03 2.114	-03 1.685	-03 1.417	-03				
1	14	1.892	-03 1.737	-03 1.601	-03 1.510	-03 1.375	-03 1.256	-03 9.643	-04 8.083	-04 6.880	-04 6.266	-04				
1	15	1.217	-01 1.273	-01 1.332	-01 1.376	-01 1.452	-01 1.529	-01 1.746	-01 1.873	-01 1.981	-01 2.066	-01				
2	3	5.851	-02 5.392	-02 5.013	-02 4.771	-02 4.435	-02 4.161	-02 3.528	-02 3.144	-02 2.749	-02 2.371	-02				
2	4	1.913	-00 1.992	-00 2.036	-00 2.111	-00 2.156	-00 2.214	-00 2.356	-00 2.436	-00 2.507	-00 2.572	-00				
2	5	1.062	+01 1.097	+01 1.119	+01 1.155	+01 1.178	+01 1.208	+01 1.280	+01 1.322	+01 1.358	+01 1.394	+01				
2	6	1.182	-02 1.048	-02 9.342	-03 8.601	-03 7.549	-03 6.689	-03 4.874	-03 4.012	-03 3.257	-03 2.560	-03				
2	7	6.286	-00 6.476	-00 6.656	-00 6.886	-00 7.011	-00 7.224	-00 7.693	-00 7.958	-00 8.194	-00 8.415	-00				
2	8	7.439	-03 6.475	-03 5.663	-03 5.143	-03 4.417	-03 3.841	-03 2.720	-03 2.259	-03 1.896	-03 1.590	-03				
2	9	2.430	-03 2.111	-03 1.850	-03 1.685	-03 1.461	-03 1.287	-03 9.501	-04 7.965	-04 6.565	-04 5.278	-04				
2	10	2.725	-01 2.736	-01 2.736	-01 2.755	-01 2.768	-01 2.791	-01 2.857	-01 2.886	-01 2.895	-01 2.881	-01				
2	11	6.269	-01 6.275	-01 6.276	-01 6.312	-01 6.335	-01 6.382	-01 6.518	-01 6.575	-01 6.584	-01 6.544	-01				
2	12	1.751	-02 1.538	-02 1.354	-02 1.234	-02 1.063	-02 9.225	-03 6.328	-03 5.080	-03 4.120	-03 3.345	-03				
2	13	4.336	-01 4.323	-01 4.335	-01 4.358	-01 4.370	-01 4.398	-01 4.484	-01 4.520	-01 4.529	-01 4.505	-01				
2	14	1.250	-02 1.093	-02 9.582	-03 8.707	-03 7.469	-03 6.463	-03 4.427	-03 3.573	-03 2.932	-03 2.440	-03				
2	15	7.907	-03 6.944	-03 6.124	-03 5.590	-03 4.836	-03 4.221	-03 2.953	-03 2.396	-03 1.959	-03 1.621	-03				



3	4	2.737	-03	2.285	-03	1.921	-03	1.697	-03	1.402	-03	1.186	-03	8.262	-04	6.968	-04	5.888	-04	4.975	-04
3	5	1.230	-02	1.075	-02	9.445	-03	8.604	-03	7.426	-03	6.482	-03	4.604	-03	3.800	-03	3.147	-03	2.575	-03
3	6	3.619	-00	3.740	-00	3.854	-00	3.942	-00	4.057	-00	4.158	-00	4.406	-00	4.517	-00	4.641	-00	4.760	-00
3	7	7.011	-03	6.174	-03	5.464	-03	5.004	-03	4.357	-03	3.833	-03	2.761	-03	2.281	-03	1.881	-03	1.528	-03
3	8	2.079	-00	2.142	-00	2.214	-00	2.277	-00	2.338	-00	2.401	-00	2.553	-00	2.631	-00	2.707	-00	2.780	-00
3	9	6.380	-01	6.650	-01	6.892	-01	7.057	-01	7.308	-01	7.534	-01	8.139	-01	8.392	-01	8.690	-01	8.963	-01
3	10	7.595	-03	6.667	-03	5.876	-03	5.360	-03	4.631	-03	4.038	-03	2.835	-03	2.324	-03	1.935	-03	1.631	-03
3	11	1.749	-02	1.539	-02	1.359	-02	1.241	-02	1.072	-02	9.324	-03	6.432	-03	5.178	-03	4.210	-03	3.424	-03
3	12	1.975	-01	1.993	-01	2.012	-01	2.028	-01	2.053	-01	2.079	-01	2.143	-01	2.167	-01	2.176	-01	2.164	-01
3	13	1.198	-02	1.046	-02	9.160	-03	8.319	-03	7.133	-03	6.173	-03	4.252	-03	3.458	-03	2.871	-03	2.436	-03
3	14	1.343	-01	1.348	-01	1.360	-01	1.373	-01	1.384	-01	1.399	-01	1.439	-01	1.454	-01	1.459	-01	1.452	-01
3	15	8.801	-02	8.963	-02	9.114	-02	9.221	-02	9.424	-02	9.613	-02	1.008	-01	1.025	-01	1.031	-01	1.025	-01
4	5	1.998	-01	1.955	-01	1.917	-01	1.896	-01	1.863	-01	1.837	-01	1.785	-01	1.760	-01	1.737	-01	1.717	-01
4	6	7.387	-03	6.826	-03	6.348	-03	6.035	-03	5.586	-03	5.211	-03	4.356	-03	3.899	-03	3.481	-03	3.112	-03
4	7	1.989	-02	1.837	-02	1.682	-02	1.603	-02	1.453	-02	1.331	-02	1.051	-02	9.161	-03	8.119	-03	7.336	-03
4	8	2.578	-03	2.276	-03	2.018	-03	1.852	-03	1.617	-03	1.430	-03	1.081	-03	9.751	-04	9.443	-04	9.863	-04
4	9	4.599	-03	4.163	-03	3.795	-03	3.558	-03	3.229	-03	2.970	-03	2.486	-03	2.317	-03	2.216	-03	2.164	-03
4	10	2.709	-00	2.821	-00	2.869	-00	2.975	-00	3.029	-00	3.110	-00	3.326	-00	3.444	-00	3.549	-00	3.648	-00
4	11	3.741	-02	3.663	-02	3.613	-02	3.592	-02	3.579	-02	3.590	-02	3.686	-02	3.751	-02	3.786	-02	3.782	-02
4	12	6.530	-03	5.698	-03	4.988	-03	4.527	-03	3.875	-03	3.347	-03	2.284	-03	1.851	-03	1.547	-03	1.350	-03
4	13	4.705	-03	3.858	-03	3.182	-03	2.784	-03	2.251	-03	1.863	-03	1.202	-03	1.035	-03	1.154	-03	1.816	-03
4	14	1.503	-03	1.276	-03	1.084	-03	9.595	-04	7.844	-04	6.442	-04	3.741	-04	2.755	-04	2.158	-04	1.864	-04
4	15	5.769	-03	4.967	-03	4.302	-03	3.880	-03	3.302	-03	2.851	-03	1.990	-03	1.639	-03	1.375	-03	1.200	-03
5	6	6.683	-02	6.073	-02	5.546	-02	5.200	-02	4.704	-02	4.295	-02	3.449	-02	3.101	-02	2.870	-02	2.747	-02
5	7	9.167	-01	8.974	-01	8.857	-01	8.783	-01	8.671	-01	8.597	-01	8.501	-01	8.498	-01	8.516	-01	8.549	-01
5	8	5.532	-02	5.012	-02	4.558	-02	4.256	-02	3.819	-02	3.454	-02	2.704	-02	2.417	-02	2.262	-02	2.225	-02
5	9	7.369	-03	6.887	-03	6.478	-03	6.211	-03	5.825	-03	5.492	-03	4.634	-03	4.071	-03	3.483	-03	2.910	-03
5	10	1.150	-01	1.147	-01	1.143	-01	1.155	-01	1.158	-01	1.171	-01	1.220	-01	1.248	-01	1.269	-01	1.286	-01
5	11	1.222	+01	1.266	+01	1.295	+01	1.343	+01	1.365	+01	1.402	+01	1.500	+01	1.553	+01	1.600	+01	1.643	+01
5	12	3.585	-02	3.108	-02	2.705	-02	2.447	-02	2.085	-02	1.796	-02	1.226	-02	9.913	-03	8.164	-03	6.916	-03
5	13	2.295	-00	2.358	-00	2.422	-00	2.512	-00	2.558	-00	2.628	-00	2.819	-00	2.922	-00	3.017	-00	3.106	-00
5	14	1.882	-02	1.618	-02	1.397	-02	1.257	-02	1.063	-02	9.096	-03	6.155	-03	4.979	-03	4.140	-03	3.633	-03
5	15	1.251	-02	1.073	-02	9.255	-03	8.322	-03	7.041	-03	6.040	-03	4.137	-03	3.388	-03	2.882	-03	2.662	-03

6	7	5-535	-02	5-011	-02	4-554	-02	4-251	-02	3-814	-02	3-452	-02	2-713	-02	2-434	-02	2-283	-02	2-251	-02
6	8	2-889	-01	2-844	-01	2-816	-01	2-807	-01	2-780	-01	2-767	-01	2-759	-01	2-770	-01	2-779	-01	2-790	-01
6	9	5-169	-02	5-166	-02	5-170	-02	5-176	-02	5-191	-02	5-211	-02	5-271	-02	5-286	-02	5-277	-02	5-236	-02
6	10	1-186	-02	1-026	-02	8-920	-03	8-060	-03	6-863	-03	5-912	-03	4-048	-03	3-289	-03	2-741	-03	2-392	-03
6	11	3-529	-02	3-036	-02	2-625	-02	2-363	-02	2-000	-02	1-714	-02	1-163	-02	9-398	-03	7-761	-03	6-691	-03
6	12	4-068	-00	4-215	-00	4-363	-00	4-480	-00	4-602	-00	4-726	-00	5-054	-00	5-197	-00	5-356	-00	5-503	-00
6	13	1-883	-02	1-641	-02	1-435	-02	1-301	-02	1-113	-02	9-616	-03	6-581	-03	5-331	-03	4-426	-03	3-809	-03
6	14	7-684	-01	7-938	-01	8-232	-01	8-490	-01	8-707	-01	8-959	-01	9-616	-01	9-928	-01	1-025	-00	1-054	-00
6	15	2-230	-02	2-281	-02	2-339	-02	2-385	-02	2-462	-02	2-540	-02	2-750	-02	2-847	-02	2-909	-02	2-930	-02
7	8	2-680	-02	2-428	-02	2-215	-02	2-078	-02	1-884	-02	1-729	-02	1-420	-02	1-292	-02	1-199	-02	1-135	-02
7	9	2-501	-03	2-309	-03	2-142	-03	2-031	-03	1-867	-03	1-724	-03	1-383	-03	1-197	-03	1-031	-03	8-927	-04
7	10	2-232	-00	2-308	-00	2-367	-00	2-457	-00	2-500	-00	2-570	-00	2-751	-00	2-849	-00	2-937	-00	3-021	-00
7	11	8-945	-02	8-645	-02	8-425	-02	8-309	-02	8-175	-02	8-109	-02	8-106	-02	8-133	-02	8-109	-02	8-029	-02
7	12	1-357	-02	1-171	-02	1-014	-02	9-140	-03	7-747	-03	6-642	-03	4-497	-03	3-641	-03	3-034	-03	2-657	-03
7	13	6-738	-00	6-917	-00	7-133	-00	7-399	-00	7-528	-00	7-732	-00	8-274	-00	8-565	-00	8-831	-00	9-077	-00
7	14	1-999	-02	1-747	-02	1-532	-02	1-393	-02	1-195	-02	1-035	-02	7-122	-03	5-776	-03	4-774	-03	4-027	-03
7	15	6-634	-03	5-693	-03	4-909	-03	4-411	-03	3-724	-03	3-184	-03	2-141	-03	1-715	-03	1-403	-03	1-208	-03
8	9	1-994	-03	1-850	-03	1-732	-03	1-656	-03	1-547	-03	1-458	-03	1-228	-03	1-046	-03	8-548	-04	6-659	-04
8	10	5-909	-03	5-100	-03	4-425	-03	3-995	-03	3-401	-03	2-931	-03	2-012	-03	1-624	-03	1-324	-03	1-114	-03
8	11	1-360	-02	1-172	-02	1-014	-02	9-130	-03	7-733	-03	6-628	-03	4-490	-03	3-634	-03	3-031	-03	2-681	-03
8	12	2-008	-02	2-028	-02	2-056	-02	2-084	-02	2-137	-02	2-195	-02	2-363	-02	2-447	-02	2-496	-02	2-509	-02
8	13	1-980	-02	1-726	-02	1-511	-02	1-372	-02	1-176	-02	1-020	-02	7-094	-03	5-833	-03	4-923	-03	4-300	-03
8	14	2-232	-00	2-294	-00	2-378	-00	2-458	-00	2-511	-00	2-579	-00	2-761	-00	2-851	-00	2-939	-00	3-020	-00
8	15	6-978	-01	7-225	-01	7-499	-01	7-728	-01	7-961	-01	8-208	-01	8-826	-01	9-159	-01	9-473	-01	9-761	-01
9	10	5-743	-03	4-947	-03	4-284	-03	3-862	-03	3-281	-03	2-826	-03	1-953	-03	1-596	-03	1-323	-03	1-124	-03
9	11	6-694	-03	5-827	-03	5-094	-03	4-622	-03	3-961	-03	3-430	-03	2-375	-03	1-948	-03	1-658	-03	1-510	-03
9	12	8-789	-03	9-044	-03	9-322	-03	9-542	-03	9-915	-03	1-029	-02	1-170	-02	1-170	-02	1-193	-02	1-196	-02
9	13	1-649	-03	1-395	-03	1-184	-03	1-051	-03	8-674	-04	7-246	-04	4-584	-04	3-614	-04	3-053	-04	2-968	-04
9	14	8-629	-04	7-468	-04	6-502	-04	5-887	-04	5-037	-04	4-365	-04	3-045	-04	2-475	-04	2-036	-04	1-735	-04
9	15	9-067	-01	9-475	-01	9-806	-01	1-002	-00	1-033	-00	1-063	-00	1-130	-00	1-158	-00	1-192	-00	1-224	-00

Effective collision strengths

10	1-604	-01 1-480	-01 1-374	-01 1-306	-01 1-205	-01 1-121	-01 9-245	-02 8-338	-02 7-887	-02 8-221	-02	
10	12	5-308	-02 4-759	-02 4-276	-02 3-954	-02 3-484	-02 2-268	-02 1-948	-02 1-766	-02 1-706	-02	
10	13	2-841	-01 2-690	-01 2-564	-01 2-492	-01 2-391	-01 2-312	-01 2-142	-01 2-138	-01 2-358	-01 3-012	-01
10	14	2-291	-02 2-030	-02 1-802	-02 1-652	-02 1-437	-02 1-259	-02 8-977	-03 7-599	-03 6-786	-03 6-442	-03
10	15	2-752	-02 2-436	-02 2-178	-02 2-017	-02 1-800	-02 1-635	-02 1-334	-02 1-212	-02 1-116	-02 1-048	-02
11	12	1-491	-01 1-327	-01 1-188	-01 1-097	-01 9-676	-02 8-601	-02 6-318	-02 5-414	-02 5-087	-02 5-632	-02
11	13	6-806	-01 6-535	-01 6-344	-01 6-232	-01 6-085	-01 5-983	-01 5-845	-01 5-906	-01 6-221	-01 7-016	-01
11	14	1-074	-01 9-634	-02 8-657	-02 8-001	-02 7-040	-02 6-227	-02 4-492	-02 3-785	-02 3-354	-02 3-167	-02
11	15	5-389	-02 4-839	-02 4-357	-02 4-036	-02 3-571	-02 3-182	-02 2-368	-02 2-035	-02 1-812	-02 1-670	-02
12	13	1-080	-01 9-702	-02 8-731	-02 8-080	-02 7-126	-02 6-318	-02 4-580	-02 3-853	-02 3-384	-02 3-142	-02
12	14	1-764	-01 1-749	-01 1-744	-01 1-746	-01 1-746	-01 1-752	-01 1-779	-01 1-794	-01 1-801	-01 1-802	-01
12	15	1-092	-02 1-093	-02 1-104	-02 1-118	-02 1-150	-02 1-187	-02 1-299	-02 1-355	-02 1-389	-02 1-410	-02
13	14	1-074	-01 9-607	-02 8-636	-02 8-001	-02 7-095	-02 6-353	-02 4-840	-02 4-232	-02 3-841	-02 3-658	-02
13	15	2-413	-02 2-131	-02 1-891	-02 1-733	-02 1-510	-02 1-328	-02 9-561	-03 8-082	-03 7-205	-03 6-988	-03
14	15	6-845	-02 6-783	-02 6-724	-02 6-678	-02 6-649	-02 6-626	-02 6-611	-02 6-601	-02 6-594	-02 6-578	-02

Table 5. Effective collision strengths for transitions in FE XVII. ( $a \pm b \equiv a \times 10^{\pm b}$ )

Transition <i>I</i>	<i>J</i>	Temperature (log K)																																																																																																																																																																																																																																																																																																																																																									
		5:40	5:60	5:80	6:00	6:20	6:40	6:50	6:70	6:80	6:90	7:00																																																																																																																																																																																																																																																																																																																																															
1	2	3-760	-02 3-358	-02 2-794	-02 2-206	-02 1-695	-02 1-289	-02 1-122	-02 8-428	-03 7-267	-03 6-237	-03 5-324	-03 3-433	-02 3-360	-02 2-683	-02 2-304	-02 2-212	-02 1-968	-02 1-816	-02 1-647	-02 1-468	-02 1-539	-02 1-364	-02 1-165	-02 9-720	-03 8-025	-03 6-611	-03 6-011	-03 5-014	-03 4-605	-03 4-243	-03 3-919	-03 3-723	-02 3-206	-02 2-650	-02 2-149	-02 1-733	-02 1-396	-02 1-255	-02 1-027	-02 9-376	-03 8-635	-03 8-019	-03 1-546	-02 1-303	-02 1-080	-02 9-031	-03 7-789	-03 7-034	-03 6-809	-03 6-537	-03 6-412	-03 6-239	-03 5-988	-03 1-270	-02 1-099	-02 9-195	-03 7-562	-03 6-184	-03 5-060	-03 4-584	-03 3-785	-03 3-451	-03 3-153	-03 2-883	-03 1-542	-02 1-139	-02 8-361	-03 6-129	-03 4-511	-03 3-347	-03 2-896	-03 2-210	-03 1-960	-03 1-761	-03 1-603	1	9	4-448	-02 4-359	-02 4-253	-02 4-160	-02 4-089	-02 4-072	-02 4-117	-02 4-461	-02 4-834	-02 5-374	-02 6-072	1	10	2-109	-02 2-063	-02 2-003	-02 1-923	-02 1-813	-02 1-667	-02 1-579	-02 1-376	-02 1-266	-02 1-153	-02 1-039	-02 1-919	-02 1-875	-02 1-816	-02 1-736	-02 1-626	-02 1-482	-02 1-397	-02 1-209	-02 1-109	-02 1-009	-02 9-099	1	11	1-919	-02 1-875	-02 1-816	-02 1-736	-02 1-626	-02 1-482	-02 1-397	-02 1-209	-02 1-109	-02 1-009	-02 9-099	1	12	3-796	-03 3-774	-03 3-792	-03 3-855	-03 3-970	-03 4-165	-03 4-310	-03 4-760	-03 5-098	-03 5-526	-03 6-041	1	13	7-796	-03 7-583	-03 7-311	-03 6-948	-03 6-465	-03 5-840	-03 5-473	-03 4-645	-03 4-198	-03 3-741	-03 3-287	1	14	2-996	-03 2-847	-03 2-691	-03 2-513	-03 2-306	-03 2-064	-03 1-933	-03 1-653	-03 1-511	-03 1-370	-03 1-232	1	15	1-043	-01 1-059	-01 1-083	-01 1-119	-01 1-172	-01 1-255	-01 1-311	-01 1-461	-01 1-552	-01 1-650	-01 1-746	2	3	3-391	-01 2-808	-01 2-247	-01 1-768	-01 1-388	-01 1-096	-01 9-759	-02 7-730	-02 6-860	-02 6-067	-02 5-345	2	4	1-301	-00 1-295	-00 1-341	-00 1-431	-00 1-553	-00 1-698	-00 1-778	-00 1-958	-00 2-063	-00 2-177	-00 2-301	2	5	6-981	-00 7-087	-00 7-439	-00 7-992	-00 8-676	-00 9-448	-00 9-865	-00 1-078	+01 1-130	+01 1-187	+01 1-247	2	6	7-463	-02 6-338	-02 5-170	-02 4-108	-02 3-215	-02 2-488	-02 2-179	-02 1-650	-02 1-425	-02 1-223	-02 1-043	2	7	4-596	-00 4-606	-00 4-737	-00 4-981	-00 5-316	-00 5-721	-00 5-933	-00 6-285	-00 6-366	-00 6-345	-00 6-203	2	8	4-776	-02 4-039	-02 3-285	-02 2-602	-02 2-028	-02 1-561	-02 1-362	-02 1-223	-02 8-782	-03 7-487	-03 6-332	2	9	9-613	-03 8-347	-03 7-024	-03 5-809	-03 4-745	-03 3-822	-03 3-407	-03 2-662	-03 2-329	-03 2-022	-03 1-742	2	10	2-620	-01 2-623	-01 2-634	-01 2-650	-01 2-672	-01 2-699	-01 2-713	-01 2-725	-01 2-712	-01 2-677	-01 2-614	2	11	5-821	-01 5-886	-01 5-956	-01 6-028	-01 6-099	-01 6-169	-01 6-198	-01 6-203	-01 6-157	-01 6-065	-01 5-923	2	12	2-880	-02 2-784	-02 2-647	-02 2-461	-02 2-225	-02 1-937	-02 1-781	-02 1-455	-02 1-290	-02 1-129	-02 9-756	2	13	4-089	-01 4-116	-01 4-148	-01 4-184	-01 4-225	-01 4-269	-01 4-292	-01 4-331	-01 4-341	-01 4-338	-01 4-315	2	14	2-052	-02 1-980	-02 1-880	-02 1-746	-02 1-575	-02 1-372	-02 1-262	-02 1-033	-02 9-181	-03 8-065	-03 7-000	2	15	1-305	-02 1-262	-02 1-200	-02 1-114	-02 1-003	-02 8-719	-03 8-016	-03 6-574	-03 5-862	-03 5-175	-03 4-524

Effective collision strengths

3	4	2-798	-02 2-258	-02 1-745	-02 1-311	-02 9-711	-03 7-130	-03 6-091	-03 4-409	-03 3-732	-03 3-147	-03 2-643	-03
3	5	1-013	-01 8-137	-02 6-366	-02 4-897	-02 3-731	-02 2-823	-02 2-448	-02 1-822	-02 1-563	-02 1-334	-02 1-133	-02
3	6	2-297	-00 2-336	-00 2-478	-00 2-692	-00 2-945	-00 3-224	-00 3-373	-00 3-712	-00 3-912	-00 4-138	-00 4-385	-00
3	7	5-163	-02 4-326	-02 3-473	-02 2-714	-02 2-090	-02 1-592	-02 1-385	-02 1-043	-02 9-071	-03 7-942	-03 7-044	-03
3	8	1-414	-00 1-432	-00 1-496	-00 1-598	-00 1-727	-00 1-873	-00 1-948	-00 2-070	-00 2-097	-00 2-089	-00 2-041	-00
3	9	4-993	-01 5-092	-01 5-256	-01 5-481	-01 5-776	-01 6-152	-01 6-371	-01 6-853	-01 7-098	-01 7-329	-01 7-528	-01
3	10	1-454	-02 1-355	-02 1-253	-02 1-143	-02 1-018	-02 8-800	-03 8-074	-03 6-605	-03 5-886	-03 5-193	-03 4-537	-03
3	11	3-135	-02 2-952	-02 2-757	-02 2-533	-02 2-271	-02 1-973	-02 1-814	-02 1-496	-02 1-345	-02 1-205	-02 1-076	-02
3	12	1-757	-01 1-789	-01 1-822	-01 1-858	-01 1-897	-01 1-940	-01 1-965	-01 2-029	-01 2-072	-01 2-125	-01 2-186	-01
3	13	1-945	-02 1-882	-02 1-791	-02 1-666	-02 1-505	-02 1-312	-02 1-207	-02 9-896	-03 8-816	-03 7-765	-03 6-763	-03
3	14	1-222	-01 1-233	-01 1-248	-01 1-267	-01 1-289	-01 1-315	-01 1-328	-01 1-352	-01 1-358	-01 1-358	-01 1-350	-01
3	15	8-145	-02 8-220	-02 8-319	-02 8-446	-02 8-613	-02 8-828	-02 8-946	-02 9-137	-02 9-165	-02 9-116	-02 8-972	-02
4	5	3-434	-01 3-168	-01 2-905	-01 2-668	-01 2-465	-01 2-294	-01 2-219	-01 2-085	-01 2-024	-01 1-965	-01 1-907	-01
4	6	3-276	-02 2-925	-02 2-473	-02 2-023	-02 1-633	-02 1-312	-02 1-176	-02 9-428	-03 8-437	-03 7-553	-03 6-769	-03
4	7	4-163	-01 3-481	-01 2-697	-01 1-986	-01 1-420	-01 1-002	-01 8-396	-02 5-889	-02 4-930	-02 4-125	-02 3-448	-02
4	8	1-324	-02 1-114	-02 9-030	-03 7-178	-03 5-669	-03 4-465	-03 3-959	-03 3-115	-03 2-776	-03 2-491	-03 2-261	-03
4	9	1-079	-02 9-537	-03 8-372	-03 7-345	-03 6-426	-03 5-580	-03 5-184	-03 4-485	-03 4-205	-03 3-985	-03 3-826	-03
4	10	2-014	-00 2-092	-00 2-183	-00 2-294	-00 2-428	-00 2-587	-00 2-677	-00 2-877	-00 2-985	-00 3-095	-00 3-203	-00
4	11	4-182	-02 4-136	-02 4-079	-02 4-008	-02 3-929	-02 3-851	-02 3-812	-02 3-700	-02 3-607	-02 3-479	-02 3-312	-02
4	12	1-133	-02 1-090	-02 1-031	-02 9-527	-03 8-541	-03 7-393	-03 6-780	-03 5-534	-03 4-925	-03 4-337	-03 3-780	-03
4	13	9-348	-03 8-917	-03 8-326	-03 7-554	-03 6-615	-03 5-581	-03 5-075	-03 4-220	-03 3-922	-03 3-729	-03 3-634	-03
4	14	3-144	-03 2-983	-03 2-772	-03 2-506	-03 2-190	-03 1-840	-03 1-659	-03 1-307	-03 1-141	-03 9-863	-04 8-438	-04
4	15	9-711	-03 9-354	-03 8-847	-03 8-165	-03 7-307	-03 6-311	-03 5-783	-03 4-717	-03 4-199	-03 3-703	-03 3-235	-03
5	6	3-070	-01 2-671	-01 2-220	-01 1-801	-01 1-447	-01 1-158	-01 1-035	-01 8-251	-02 7-358	-02 6-558	-02 5-845	-02
5	7	2-057	-00 1-845	-00 1-618	-00 1-417	-00 1-255	-00 1-133	-00 1-084	-00 1-003	-00 9-646	-01 9-248	-01 8-804	-01
5	8	1-793	-01 1-583	-01 1-360	-01 1-152	-01 9-668	-02 8-050	-02 7-320	-02 6-020	-02 5-459	-02 4-962	-02 4-531	-02
5	9	2-435	-02 2-087	-02 1-751	-02 1-463	-02 1-228	-02 1-034	-02 9-469	-03 7-846	-03 7-064	-03 6-296	-03 5-547	-03
5	10	1-315	-01 1-263	-01 1-227	-01 1-202	-01 1-186	-01 1-180	-01 1-181	-01 1-192	-01 1-201	-01 1-210	-01 1-219	-01
5	11	8-651	-00 9-163	-00 9-696	-00 1-027	+01 1-092	+01 1-163	+01 1-197	+01 1-232	+01 1-218	+01 1-178	+01 1-111	+01
5	12	6-328	-02 6-083	-02 5-743	-02 5-292	-02 4-731	-02 4-081	-02 3-735	-02 3-034	-02 2-690	-02 2-359	-02 2-045	-02
5	13	1-870	-00 1-905	-00 2-022	-00 2-114	-00 2-229	-00 2-292	-00 2-292	-00 2-400	-00 2-424	-00 2-415	-00 2-366	-00
5	14	3-342	-02 3-208	-02 3-024	-02 2-782	-02 2-482	-02 2-135	-02 1-952	-02 1-585	-02 1-408	-02 1-239	-02 1-079	-02
5	15	2-113	-02 2-034	-02 1-922	-02 1-772	-02 1-584	-02 1-366	-02 1-250	-02 1-019	-02 9-073	-03 8-010	-03 7-013	-03

6	7	1-959	-01 1-729	-01 1-477	-01 1-238	-01 1-027	-01 8-458	-02 7-651	-02 6-217	-02 5-587	-02 5-010	-02 4-482	-02
6	8	5-894	-01 5-283	-01 4-670	-01 4-144	-01 3-734	-01 3-431	-01 3-314	-01 3-137	-01 3-063	-01 2-985	-01 2-889	-01
6	9	5-519	-02 5-408	-02 5-335	-02 5-287	-02 5-243	-02 5-243	-02 5-255	-02 5-394	-02 5-574	-02 5-861	-02 6-262	-02
6	10	4-067	-02 3-360	-02 2-797	-02 2-339	-02 1-948	-02 1-598	-02 1-435	-02 1-133	-02 9-942	-02 8-645	-03 7-446	-03
6	11	8-599	-02 7-555	-02 6-679	-02 5-877	-02 5-087	-02 4-289	-02 3-892	-02 3-128	-02 2-771	-02 2-439	-02 2-134	-02
6	12	2-916	-00 3-098	-00 3-280	-00 3-470	-00 3-682	-00 3-929	-00 4-073	-00 4-438	-00 4-680	-00 4-974	-00 5-318	-00
6	13	3-338	-02 3-210	-02 3-030	-02 2-791	-02 2-494	-02 2-153	-02 1-971	-02 1-604	-02 1-423	-02 1-249	-02 1-084	-02
6	14	6-020	-01 6-209	-01 6-429	-01 6-703	-01 7-049	-01 7-475	-01 7-705	-01 8-103	-01 8-204	-01 8-192	-01 8-045	-01
6	15	2-000	-02 2-019	-02 2-047	-02 2-088	-02 2-149	-02 2-232	-02 2-275	-02 2-319	-02 2-292	-02 2-221	-02 2-103	-02
7	8	3-471	-01 2-801	-01 2-155	-01 1-606	-01 1-177	-01 8-582	-02 7-331	-02 5-369	-02 4-609	-02 3-967	-02 3-426	-02
7	9	7-327	-03 6-173	-03 5-167	-03 4-355	-03 3-705	-03 3-159	-03 2-909	-03 2-431	-03 2-198	-03 1-968	-03 1-744	-03
7	10	1-615	-00 1-692	-00 1-778	-00 1-877	-00 1-993	-00 2-123	-00 2-185	-00 2-255	-00 2-235	-00 2-167	-00 2-050	-00
7	11	1-533	-01 1-348	-01 1-218	-01 1-122	-01 1-045	-01 9-813	-02 9-525	-02 8-916	-02 8-543	-02 8-098	-02 7-573	-02
7	12	2-474	-02 2-361	-02 2-217	-02 2-034	-02 1-811	-02 1-557	-02 1-423	-02 1-158	-02 1-033	-02 9-166	-03 8-113	-03
7	13	5-165	-00 5-327	-00 5-524	-00 5-776	-00 6-091	-00 6-477	-00 6-702	-00 7-236	-00 7-543	-00 7-863	-00 8-169	-00
7	14	3-451	-02 3-325	-02 3-147	-02 2-908	-02 2-609	-02 2-260	-02 2-073	-02 1-694	-02 1-508	-02 1-329	-02 1-160	-02
7	15	1-171	-02 1-124	-02 1-059	-02 9-718	-03 8-641	-03 7-407	-03 6-754	-03 5-429	-03 4-781	-03 4-158	-03 3-572	-03
8	9	2-791	-02 2-301	-02 1-779	-02 1-323	-02 9-652	-03 6-995	-03 5-953	-03 4-299	-03 3-640	-03 3-069	-03 2-573	-03
8	10	1-318	-02 1-203	-02 1-091	-02 9-744	-03 8-510	-03 7-216	-03 6-560	-03 5-273	-03 4-660	-03 4-077	-03 3-532	-03
8	11	3-604	-02 3-106	-02 2-706	-02 2-355	-02 2-022	-02 1-694	-02 1-533	-02 1-221	-02 1-074	-02 9-335	-03 8-028	-03
8	12	1-894	-02 1-891	-02 1-898	-02 1-918	-02 1-951	-02 2-006	-02 2-043	-02 2-143	-02 2-207	-02 2-282	-02 2-365	-02
8	13	3-510	-02 3-355	-02 3-157	-02 2-906	-02 2-599	-02 2-247	-02 2-061	-02 1-685	-02 1-501	-02 1-326	-02 1-159	-02
8	14	1-684	-00 1-751	-00 1-825	-00 1-914	-00 2-022	-00 2-150	-00 2-223	-00 2-380	-00 2-464	-00 2-552	-00 2-641	-00
8	15	5-910	-01 5-987	-01 6-110	-01 6-297	-01 6-567	-01 6-927	-01 7-129	-01 7-482	-01 7-571	-01 7-556	-01 7-417	-01
9	10	1-084	-02 1-028	-02 9-607	-03 8-784	-03 7-804	-03 6-700	-03 6-121	-03 4-960	-03 4-398	-03 3-860	-03 3-355	-03
9	11	1-438	-02 1-317	-02 1-197	-02 1-073	-02 9-407	-03 8-019	-03 7-317	-03 5-952	-03 5-314	-03 4-719	-03 4-175	-03
9	12	7-768	-03 7-726	-03 7-788	-03 7-962	-03 8-259	-03 8-694	-03 8-971	-03 9-664	-03 1-010	-02 1-059	-02 1-114	-02
9	13	4-104	-03 3-703	-03 3-314	-03 2-918	-03 2-506	-03 2-086	-03 1-879	-03 1-487	-03 1-309	-03 1-146	-03 9-991	-04
9	14	3-933	-03 3-129	-03 2-502	-03 2-014	-03 1-621	-03 1-294	-03 1-150	-03 8-919	-04 7-777	-04 6-728	-04 5-772	-04
9	15	7-445	-01 7-625	-01 7-852	-01 8-146	-01 8-524	-01 8-983	-01 9-219	-01 9-555	-01 9-581	-01 9-483	-01 9-274	-01

Effective collision strengths

10	11	2.518	-01	2.421	-01	2.302	-01	2.156	-01	1.982	-01	1.786	-01	1.682	-01	1.469	-01	1.361	-01	1.254	-01	1.148	-01
10	12	8.651	-02	8.351	-02	7.939	-02	7.393	-02	6.710	-02	5.910	-02	5.482	-02	4.614	-02	4.191	-02	3.784	-02	3.397	-02
10	13	3.578	-01	3.523	-01	3.437	-01	3.315	-01	3.158	-01	2.989	-01	2.923	-01	2.911	-01	3.001	-01	3.167	-01	3.402	-01
10	14	4.098	-02	3.929	-02	3.700	-02	3.405	-02	3.048	-02	2.645	-02	2.434	-02	2.014	-02	1.813	-02	1.622	-02	1.443	-02
10	15	4.495	-02	4.328	-02	4.097	-02	3.798	-02	3.434	-02	3.026	-02	2.814	-02	2.395	-02	2.196	-02	2.007	-02	1.831	-02
11	12	2.489	-01	2.401	-01	2.278	-01	2.115	-01	1.912	-01	1.680	-01	1.560	-01	1.338	-01	1.248	-01	1.180	-01	1.134	-01
11	13	7.906	-01	7.816	-01	7.680	-01	7.492	-01	7.255	-01	7.004	-01	6.903	-01	6.845	-01	6.921	-01	7.073	-01	7.285	-01
11	14	1.729	-01	1.673	-01	1.594	-01	1.486	-01	1.350	-01	1.189	-01	1.103	-01	9.257	-02	8.395	-02	7.571	-02	6.797	-02
11	15	8.494	-02	8.216	-02	7.821	-02	7.291	-02	6.625	-02	5.847	-02	5.429	-02	4.571	-02	4.146	-02	3.733	-02	3.338	-02
12	13	1.738	-01	1.683	-01	1.604	-01	1.496	-01	1.360	-01	1.198	-01	1.111	-01	9.320	-02	8.439	-02	7.589	-02	6.782	-02
12	14	1.790	-01	1.793	-01	1.792	-01	1.787	-01	1.780	-01	1.775	-01	1.775	-01	1.784	-01	1.796	-01	1.813	-01	1.834	-01
12	15	1.232	-02	1.214	-02	1.192	-02	1.171	-02	1.157	-02	1.158	-02	1.164	-02	1.173	-02	1.164	-02	1.138	-02	1.094	-02
13	14	1.730	-01	1.673	-01	1.593	-01	1.485	-01	1.350	-01	1.192	-01	1.107	-01	0.935	-01	0.850	-01	0.768	-01	0.689	-01
13	15	0.416	-01	0.399	-01	0.377	-01	0.347	-01	0.311	-01	0.270	-01	0.249	-01	0.206	-01	0.186	-01	0.167	-01	0.149	-01
14	15	7.265	-02	7.237	-02	7.189	-02	7.120	-02	7.034	-02	6.938	-02	6.883	-02	6.715	-02	6.572	-02	6.371	-02	6.101	-02

results ( $\gamma_{\text{our}}$ ) with that of Smith *et al* [11] ( $\gamma_s$ ) by including cascade and resonance excitation we find that for transition to higher excited states e.g.  $2p^6 1s^e \rightarrow 2p^5 3d^1 P^0$ , the value of  $\gamma$  at  $\log T_e = 6.0$  and  $\gamma_{\text{our}} \approx 0.10$  while at  $\log T_e = 7.0$  we have  $\gamma_{\text{our}} \approx 0.17$  and  $\gamma_s = 0.15$ . Thus for transition to excited states our results lie above than that obtained by Smith *et al* [11]. However, for transition to  $2p^5 3s^1 P^0$  from ground state we have  $\gamma_{\text{our}} \approx 0.03$ ,  $l_s \approx 0.11$  at  $\log T_e = 6.0$  while  $\gamma_{\text{our}} \approx 0.14$ ,  $\gamma_s \approx 0.08$  at  $\log T_e \approx 7.0$ . Thus we find that radiative cascade and resonance contributions play an insignificant role at higher temperature where *R*-matrix results are more reliable, whereas their contributions becomes important at low temperatures and for excitation to lower excited states as also shown by Smith *et al* [11]. Among the transitions from  $2p^5 3s^3 P^0$ , the largest  $\gamma$  was for the  $2p^5 3s 3P^0 \rightarrow 2p^5 3p^3 D^e$  transition. Among all the 105 transitions, the value of  $\gamma$  for  $2p^5 3p^3 D^e \rightarrow 2p^5 3d^3 F^0$  was found to be the largest, which is again dipole allowed.

Finally, since the ground state  $2s^2 2p^6 1S^e$  has no fine structure, one can easily deduce the collision strengths for transitions from this to various fine structure levels from our results in the LS coupling scheme using the following relations:

$$\gamma(^1S_0 \rightarrow (2s+1)_{LJ}) = \frac{(2J+1)}{(2L+1)(2S+1)} \gamma(^1S^e \rightarrow (2s+1)_L).$$

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