

Response surface method applied to optimization of estradiol permeation in chitosan membranes

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Abstract. The present work deals with the study of estradiol permeation in chitosan membranes. A fractional factorial design was built for the determination of the main factors affecting estradiol permeation. The independent factors analysed were: concentration of chitosan, concentration of cross-linking agent, cross-linking time and thermal treatment. It was found that concentration of chitosan and cross-linking time significantly affected the response. The effects of thermal treatment and concentration of cross-linking agent were not significant. An optimization process based on response surface methodology was carried out in order to develop a statistical model which describes the relationship between active independent variables and estradiol flux. This model can be used to find out a combination of factor levels during response optimization. Possible options for response optimization are to maximize, minimize or move towards a target value.

Keywords. Chitosan; dry heat; mass transport; membranes; water sorption.

1. Introduction

Chitosan (CHT) is an abundant, low cost, biodegradable, biocompatible and non-toxic polysaccharide with good membrane and gel forming properties. Membranes have found applications in drug delivery systems, skin permeation simulation, waste water treatment, packaging in food industry and textile dyeing (Ravi Kumar 2000; Stamatialis *et al* 2008).

CHT membranes prepared by a casting solvent evaporation technique can be obtained at ambient or higher temperature. A higher temperature reduces time needed for solvent evaporation. Thermal treatment of freshly formed membranes can be an alternative method of altering the structure, decreasing solubility and increasing the strength. Various processes including amidation, degradation and cross-linking of polymeric chains take place during thermal treatment (Zotkin *et al* 2004). Lim and Wan (1995) reported that heat treatment decreased the extent of swelling and dissolution of CHT films in aqueous media. Retuert *et al* (2000) suggested that films hardness increases with a moderate heating (60.0°C) after 1 h. Ritthidej *et al* (2002) evaluated physico-chemical change of films after moist heat treatment and concluded that water sorption and dissolution of the films were decreased after treatment. Bernabé *et al* (2005) studied the effect of thermal cross-linking on swelling behaviour of CHT/pectin polyelectrolyte complex membranes. The thermally treated membranes were stable in strong acid and basic media and swelling decreased as the time of thermal

treatment increased. Moreover, the effect of heat treatment was studied on other polymers than CHT. Pongjanyakul *et al* (2006) studied the effect of heat treatment (65°C) on drug release from glyceryl palmitostearate–alginate beads.

CHT membrane properties can also be modified by cross-linking reactions. Cross-linking is a process where polymeric chains are linked either by covalent bonds or by physical interactions between the polymer and the cross-linking agent or between the polymers themselves. A cross-linking reaction can increase chemical stability and stiffness, alter permeability, absorption capacity and colour (Neto *et al* 2005). According to Berger *et al* (2004), cross-linking density is defined as the ratio of moles of cross-linking agent to the moles of polymer repeating units. The cross-linking agent tripolyphosphate can possess a high charge density and it is able to diffuse into CHT membranes. Its use as ionic cross-linking agent has been extensively reported (Shu and Zhu 2002; Mengatto *et al* 2010).

Experimental design and optimization are tools that are used to systematically examine different types of problems that arise within research, development and production. A screening experiment is performed in order to determine the experimental variables and interactions that have significant influence on the response. The goal in any optimization is to find out the conditions that produce the desired response. Statistical methods, including response surface methodology and artificial neural networks, are used in developing and optimizing polymeric systems for a wide range of applications (Dureja *et al* 2001; Rana *et al* 2004, 2005; Leonardi *et al* 2008; Khayet *et al* 2010). Estradiol (E2) is a female hormone. Whether as hormonal

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contraception throughout the reproductive years or as hormone therapy at menopause, E2 is widely used. This hormone is also a contaminant present in waste water effluent.

Membrane technology involves the knowledge about polymer membranes and drug relationships. Essentially, based on permeation aspects, molecules can diffuse through the polymer or through water-filled pores. Interactions between the molecules to be diffused and the polymer, such as hydrogen bonds, should be considered (Banasiak and Schäfer 2010). Moreover, dissolution, erosion and water sorption or swelling can contribute to the permeation process. Several hormones were studied in applications concerning membranes. Controlled release systems where human growth hormone was incorporated into a polymer matrix (Fredenberg *et al* 2011) and ethinylestradiol was included into a reservoir placed between a drug impermeable layer and a membrane were developed (Gao *et al* 2009). The purification and separation of insulin is an important step in pharmaceutical industry. Planned membrane design leads to the preparation of membranes which are promising filter candidates for size-exclusion separation (Akbache *et al* 2009; El-Safty and Shenashena 2011). The retention of micropollutants such as estrone from water is an important issue with regard to wastewater treatment and involves membrane filtration technology (Schäfer *et al* 2010). Nghiem *et al* (2004) investigated recycling of domestic waste water effluent using thin-film composite nanofiltration membranes for the removal of E2 and its metabolite estrone. They concluded that the transport mechanism of E2 through the membrane is diffusion rather than convection; however, the role of water in facilitating this transport remains unclear. Braeken *et al* (2005) reported that E2 retention in nanofiltration was lower than expected, based on the molecular weight cut-off of membranes. The interaction between E2 and CHT was studied in a previous work (Mengatto *et al* 2010). The results suggested that the existence of pore filled water inside the polymeric membrane may contribute to E2 diffusion because of its hydrophobicity and less solvation. As noted, some of the uses of CHT membranes are waste water treatment and the development of drug delivery systems. For these reasons it is important to increase knowledge on the E2 flux through CHT cross-linked membranes focusing on the development of a model which describes the relationship between membrane formulation variables and E2 flux.

The aim of this study was to determine the influence of four preparation parameters of CHT membranes on E2 flux, and then develop a statistical model which could be used to find out the experimental combinations of factors to prepare membranes for different potential applications.

2. Experimental

2.1 Material

CHT was purchased from Polymar (Brazil). Sodium tripolyphosphate (TPP) and E2 (purity 99%) were purchased from Sigma (US). Acetonitrile was HPLC grade (Merck,

Germany). Acetic acid and ethanol were both PA>99.5% (Cicarelli, Argentina). Isotonic phosphate buffer saline (PBS, pH 7.4) was prepared by dissolving 8 g of NaCl, 0.2 g of KCl, 0.2 g of KH₂PO₄ and 1.44 g of Na₂HPO₄·2H₂O in 1 l of water. Sodium chloride, potassium chloride, potassium phosphate monobasic, sodium phosphate dibasic dehydrate and sodium acetate (Anedra, Argentina) were of analytical grade.

Experimental design and data analysis were performed with software Stat-Ease Design-Expert trial Version 7.0. Results were considered statistically significant if $p < 0.05$.

2.2 Characterization of chitosan powder

The degree of deacetylation (DD) was determined from elemental analysis. Carbon (%C), hydrogen (%H) and nitrogen (%N) contents in CHT samples were measured on an Exeter CE 440 elemental analyser. The DD was calculated from nitrogen-carbon ratio according to (1) reported by Dong *et al* (2001)

$$\frac{\%N}{\%C} = \frac{14}{96 - 24DD} \quad (1)$$

The weight average molecular weight (\bar{M}_w) was determined from static light scattering measurement. A multi angle laser light scattering photometer from Brookhaven Instruments was used. CHT solutions were prepared in 0.2 M acetic acid/0.1 M sodium acetate aqueous solution and filtered through glass filter and membrane filter of 0.2 μm . The experiments were carried out over an angular range from 30° to 150° at 632.8 nm and ambient temperature. Data were analysed by the Zimm plot method (Wang *et al* 1991).

2.3 Quantification of estradiol by HPLC — Evaluation of the method performance

The HPLC instrumentation (Shimadzu model LC-10) consisted of a ternary team of high-performance liquid chromatography with UV detection by diode array. The chromatographic system and conditions of analysis were performed, assembling US Pharmacopoeia recommendations for E2 (USP 2007), as follows: C18 column (Spherisorb ODS2, 250×4.6 mm, 5 mm internal diameter), mobile phase acetonitrile:water (50:50), flow rate 1 ml min⁻¹, oven temperature 30°C, wavelength 280 nm, stop time 8 min and injection manual volume 20 μl .

E2 was dissolved in ethanol (300 $\mu\text{g ml}^{-1}$) and stored (4°C) in darkness condition as stock solution. The standard solutions for the evaluation of the analytical method performance were prepared by dilution of an exact volume of the stock solution in ethanol:PBS (40:60). The standard solutions were filtered through a membrane filter of 0.45 μm .

In order to verify the linearity of the analytical procedure within a concentration range of 0.5–100 $\mu\text{g ml}^{-1}$ of E2, seven concentration levels were prepared and analysed three times each. The calibration curve (peak area vs E2 concentration) was fitted to a straight line, using linear

regression analysis. The precision of the procedure expressed as the coefficient of variation (CV%) was determined by the analysis within same day of six replicates of three standard solutions at three levels of concentration (3.0, 10.0 and 50.0 $\mu\text{g ml}^{-1}$). Intermediate precision (CV%) was also determined to evaluate variations between different days. Six replicates of 25.0 $\mu\text{g ml}^{-1}$ of E2 concentration were analysed on three different days (ICH 2005).

2.4 Preparation of cross-linked chitosan membranes

CHT membranes were obtained by a casting solvent evaporation technique. Polymer solutions (3 and 4% w/v) were prepared by dissolving CHT in a 2 M acetic acid solution. A portion was poured on a polycarbonate Petri dish and subjected to drying at room temperature until constant weight. The dried membranes were stored in polyethylene bags till use, but for a maximum of 7 days. Bags were kept in a closed container under darkness condition. Circular sections of the dried membranes (5 cm^2) were cut and subjected to dry thermal treatment (60°C–60 min). Subsequently, they were cross-linked by dipping in a TPP solution (10 ml–5% w/v) for 15 min and introduced into bottles having 10 ml of ethanol:PBS solution (40:60). At predetermined times the membranes were taken out; excess water was removed carefully with filter paper from the membrane surface, and then weighed immediately. This procedure was repeated until the membranes reached constant weight. Equilibrium water content (EWC) and swelling ratio (SR) were calculated according to the following equations (Shu and Zhu 2002; El-Sherbiny and Smyth 2010), respectively:

$$\text{EWC}(\text{g g}^{-1}) = \frac{W_s - W_0}{W_s}, \quad (2)$$

$$\text{SR} = \frac{W_s}{W_0}, \quad (3)$$

where W_0 is the initial dry weight and W_s the swollen equilibrium weight.

The same cross-linking and EWC evaluation procedures were performed for membranes without thermal treatment. The thickness of cross-linked membranes with and without thermal treatment was determined with a micrometer. The thickness was measured in five places of the circular sections.

2.5 In vitro diffusion experiments

In order to determine the main factor affecting E2 flux, a fractional factorial design (2^{4-1}) at two levels was built. The independent factors analysed were: concentration of CHT (3 and 4% w/v), concentration of cross-linking agent (5 and 10% w/v), cross-linking time (15 and 45 min) and thermal treatment (with or without exposure to 60°C–60 min). The factors showing significant effects were then considered for a central composite design (CCD) consisting of 12 experiments in order to develop a statistical model. All CHT

membranes were prepared following the methodology reported in § 2.4.

Diffusion experiments were conducted using a vertical Franz diffusion cell (PermeGear Inc. US). The receptor fluid was thermostatically regulated to 37°C under moderate stirring. Firstly, a freshly cross-linked membrane was clamped between donor and receptor compartments. The membrane was allowed to equilibrate overnight with diffusion medium. The donor fluid was exchanged with a fresh donor solution containing E2 (500 $\mu\text{g ml}^{-1}$) in 40:60 ethanol:PBS mixture. Aliquots (200 μl) were withdrawn from the receptor compartment and assayed by HPLC. An equal volume of fresh medium was added to maintain a constant volume.

E2 flux was calculated from the slope of the linear portion of the cumulative amount permeated per unit area vs time plots.

2.6 Morphology observation

The surface and cross-section morphology of cross-linked membranes were observed. Cross-section samples were prepared by fracturing cross-linked membranes after immersion in liquid nitrogen. Several samples were mounted on metal grids and coated with gold using a Sputter/Carbon coating system (SPI Supplies). Coated samples were observed using a JEOL JSM-35C scanning electron microscope.

3. Results and discussion

The functional, physical and chemical properties of CHT depend on its molecular weight and DD. Therefore, the determination of these parameters should be one of the routine analyses performed when CHT is used. The DD determined from elemental analysis was 73.0% and the \overline{M}_w determined from static light scattering measurement was 285 kDa.

Before permeation study, an analytical method for drug quantification should be developed and evaluated. The evaluation of performance of the method showed that the model can explain $\sim 99.98\%$ (R^2) of the variation in the response variable. The corresponding correlation coefficient (R) was 0.9999 and indicated a large relationship between the variables. The p -value of the model was smaller than 0.05 ($p = 0.0000$) and indicated a statistically significant relationship between peak area and E2 concentration for a significance level of 95.0%. The p -value of the lack-of-fit was higher than 0.05 ($p = 0.6011$) and indicated that the proposed lineal model fitted well for a significance level of 95.0%. The precision of the procedure was determined by the analysis within same day of six replicates of three standard solutions at three levels of concentration. CV values were smaller than 2.0% and indicated good precision. CV values for each level of concentration were 1.87% (3.0 $\mu\text{g ml}^{-1}$), 1.71% (10.0 $\mu\text{g ml}^{-1}$) and 0.81% (50.0 $\mu\text{g ml}^{-1}$). Intermediate precision was also good (CV = 2.92%). Good results obtained with respect to linearity and precision indicated that the analytical procedure can be used to quantify E2.

All the cross-linked membranes retained their flexibility and integrity in the ethanol:PBS mixture and were translucent.

Table 1 shows swelling experimental results. Thermal treatment significantly decreased weight after cross-linking, EWC and SR in comparison with non-exposed membranes ($p < 0.05$). This result agrees with that reported by Bernabé *et al* (2005). Water loss and more close interactions between polymeric chains are proposed as explanation. However, thermal treatment had no effect on the thickness after cross-linking ($p > 0.05$). According to this result, thermal treatment was included in statistical screening to evaluate its effect on E2 permeation.

To find out the main factors affecting E2 flux, a two-level fractional factorial design was built. Table 2 shows independent factor combinations and response values. The analysis of variance (ANOVA) showed that model ($p = 0.0003$), concentration of CHT ($p = 0.0001$) and cross-linking time ($p = 0.0002$) were significant. Effects were considered statistically significant due to p -value which was smaller than 0.05. The response decreased as the concentration of polymer increased. E2 flux increased with an increase in cross-linking time. The effects of concentration of cross-linking agent ($p = 0.3277$) and thermal treatment ($p = 0.9031$) were not significant. It has been proposed that drug diffusion may decrease, with more cross-linked sites formed due to prolongation of cross-linking time or increase in concentration of cross-linking agent (Berger *et al* 2004). In this work, E2 flux increased with an increase in cross-linking time and an

increase in concentration of cross-linking agent, although the effect of the second was not significant. These results were in agreement with Rana *et al* (2004, 2005) who reported an increase in the flux of 5-fluorouracil and indomethacin with an increase in concentration of cross-linking agent. For the system under study, the relation between E2 hydrophobicity and CHT hydrophilicity was proposed as explanation (Mengatto *et al* 2010). Figure 1 shows normal probability plot and Pareto chart. The normal plot probability indicates whether the residuals follow a normal distribution. Significant effects show up as deviations from the straight line. Concentration of CHT and cross-linking time deviated from normality. Similar conclusions were achieved with the Pareto chart. Effects of concentration of CHT and cross-linking time were above the Bonferroni limit and were almost certainly significant. Although thermal treatment decreased EWC (table 1), the effect was not significant. Temperature and duration of heat treatment determine the degree of heat induced changes. More drastic treatment conditions could result in a significant effect on drug flux. Three replicates of two membranes randomly selected from fractional factorial design were analysed. CV values obtained for E2 flux evaluated at steady state were lower than 10% and indicated good reproducibility (Chilcott *et al* 2005). Figure 2 shows amount of E2 diffused through CHT membranes as a function of time. Over a time, the flux approached a steady-state value and the cumulative amount penetrating the membrane increased linearly in time. However, time (lag time) was

Table 1. Swelling experimental results.

	CHT 3 (% w/v)		CHT 4 (% w/v)	
	Without TT	With TT	Without TT	With TT
Weight after CL (g)	0.1661(0.0002)	0.1474(0.0006)	0.2852(0.0009)	0.2449(0.0003)
Thickness after CL (μm)	217(6)	213(6)	323(7)	327(6)
EWC (g g^{-1})	0.286(0.005)	0.274(0.005)	0.316(0.004)	0.302(0.003)
SR	1.401(0.0013)	1.372(0.007)	1.462(0.010)	1.434(0.007)

CHT: chitosan, TT: thermal treatment, CL: cross-linking, EWC: equilibrium water content, SR: swelling ratio, SD in parentheses ($n \geq 3$).

Table 2. Fractional factorial design used in study of variables affecting E2 flux.

Experiment	Factors				Response
	Concentration of CHT (% w/v)	Concentration of TPP (% w/v)	Cross-linking time (min)	Thermal treatment	E2 flux ($\mu\text{g cm}^{-2} \text{h}^{-1}$)
1	3	10	15	With	5.8625
2	4	5	15	With	2.3700
3	4	5	45	Without	4.8743
4	4	10	45	With	5.2806
5	3	10	45	Without	13.2250
6	3	5	15	Without	5.8000
7	4	10	15	Without	2.5538
8	3	5	45	With	13.2570

CHT: chitosan, TPP: sodium tripolyphosphate, E2: estradiol.

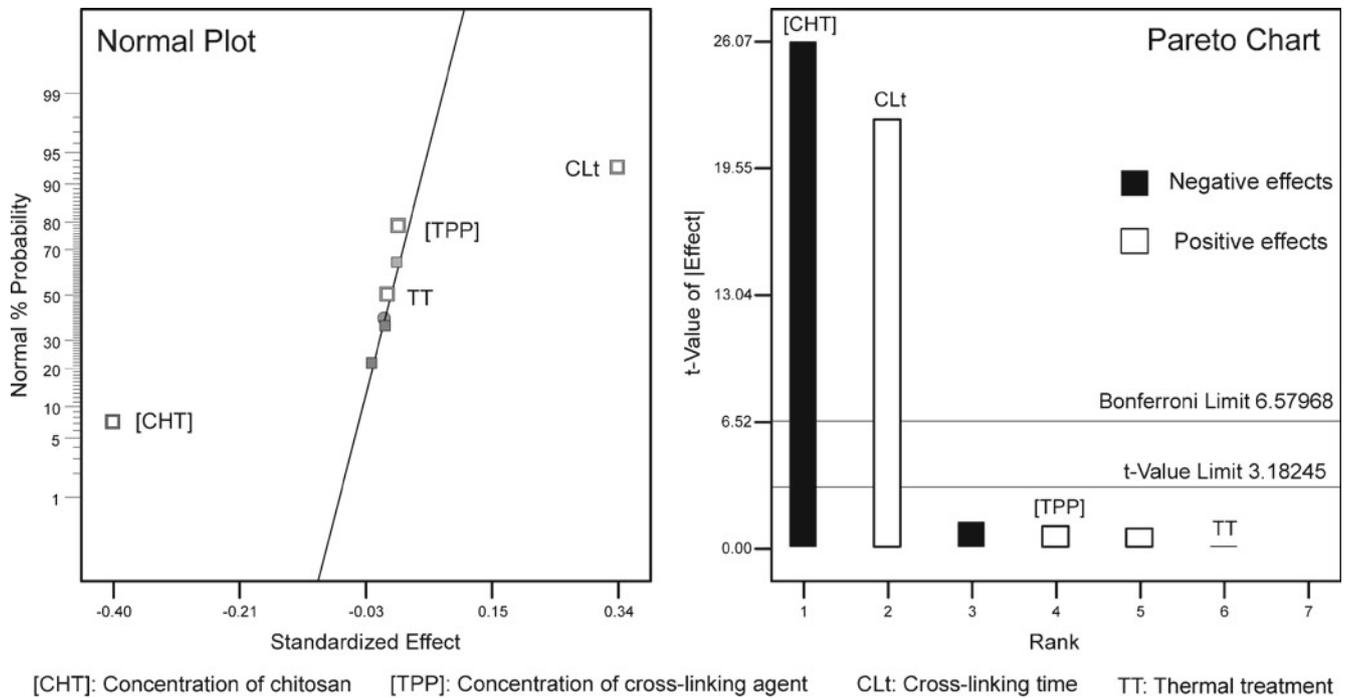


Figure 1. Normal probability plot and Pareto chart.

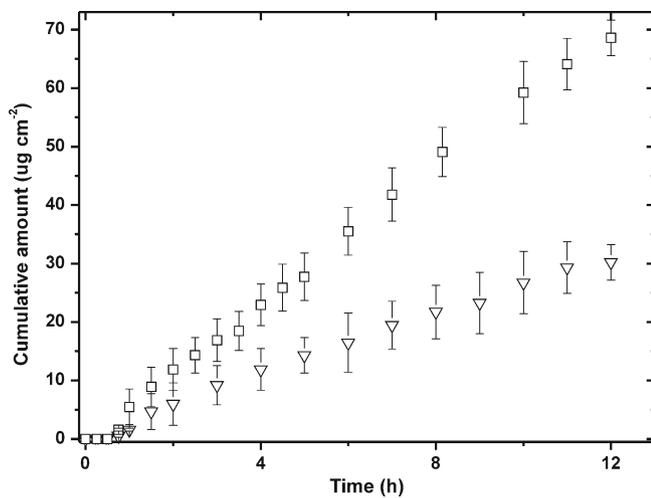


Figure 2. Cumulative amount permeated per unit area vs time plots. Membranes were prepared according to factors combination of experience number 1 (square) and number 7 (triangle) of fractional factorial design.

required after initial contact with membranes for such a steady state to be achieved.

Table 3 shows independent factor combinations and response values of CCD. Due to the fact that the effect of concentration of cross-linking agent was not significant, for membrane preparation, low level of this factor was selected. Then, membranes were cross-linked by dipping in a 5% w/v TPP solution. A lineal model was proposed and the model coefficients were validated by ANOVA. The p -value of the model was smaller than 0.05 ($p = 0.0046$) and indicated that

Table 3. Central composite design.

Experiment	Concentration of CHT (% w/v)	Cross-linking time (min)	E2 flux ($\mu\text{g cm}^{-2} \text{h}^{-1}$)
1	3.50	30.00	7.7658
2	4.34	30.00	2.4571
3	2.66	30.00	15.2280
4	3.50	55.23	12.7430
5	4.00	15.00	2.5744
6	3.50	30.00	5.7227
7	3.50	30.00	9.6351
8	3.50	30.00	9.0805
9	3.50	4.77	9.7409
10	3.00	45.00	11.1690
11	3.00	15.00	6.4650
12	4.00	45.00	4.1327

CHT: chitosan, E2: estradiol.

the model terms were significant. The p -value of the lack-of-fit was not significant ($p = 0.2553 > 0.05$) and indicated that the proposed lineal model fitted well for a significance level of 95%. The model can explain $\sim 70.11\%$ (R^2) of the variation in the response variable and can be used to navigate the design space. The final equation of the statistical model developed is:

$$\text{E2 flux} = 29.1728 - 6.7113 \cdot [\text{CHT}] + 0.079119 \cdot \text{CLt}, \quad (4)$$

where [CHT] is concentration of CHT (% w/v) and CLt is cross-linking time (min).

This model can be used to find out a combination of factor levels to prepare membranes with definite fluxes. Figure 3 shows a three-dimensional response surface plot of E2 flux,

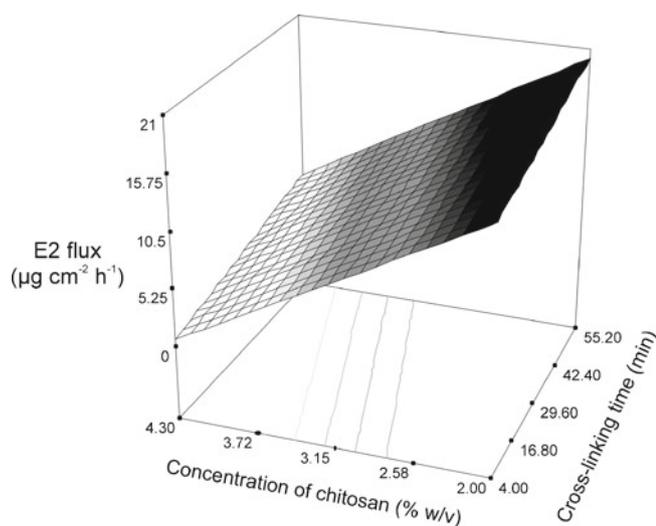


Figure 3. Response surface plot of estradiol (E2) flux.

based on the first-order model using concentration of CHT and cross-linking time as independent variables. Because the model is first-order, the fitted response surface is a plane. Based on examination of this fitted surface, it is clear that E2 flux increases as cross-linking time increases and concentration of CHT decreases. Often a fitted surface such as this can be used to determine an appropriate direction of potential improvement for the response.

Figure 4 shows micrographs of the cross-sections (figures 4a and b) and surfaces (figures 4c and d) of cross-linked membranes. The cross-section micrographs show a dense, compact and homogeneous structure for membranes prepared from concentration of CHT of 2.66% w/v (figure 4a) and 3.5% w/v (figure 4b). The surface micrographs show a relatively rough structure for membranes prepared from concentration of CHT of 2.66% w/v (figure 4c) and 3.5% w/v (figure 4d). These membranes were prepared with 5% w/v concentration of cross-linking agent and 30 min of cross-linking time (according to CCD). As the membranes prepared in this work were dense rather than porous, additional information could not be obtained from morphological observation.

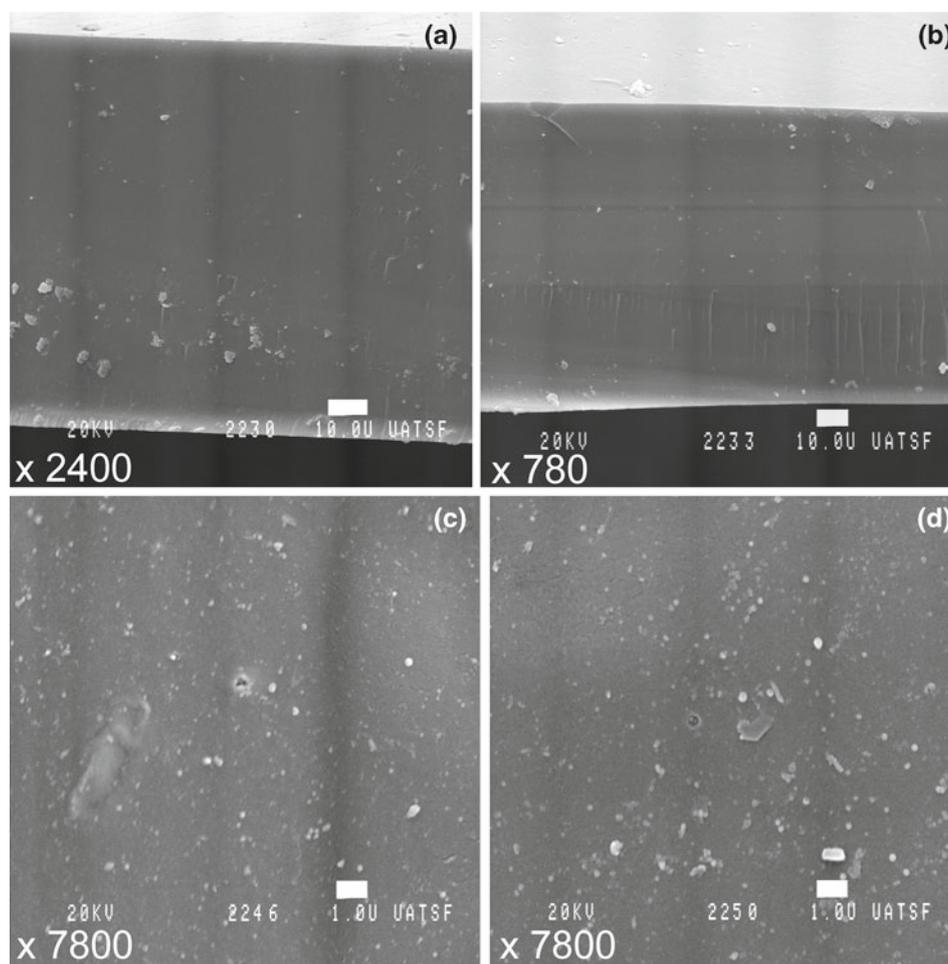


Figure 4. Morphology of cross-sections (a and b) and surfaces (c and d) of cross-linked membranes prepared from a concentration of chitosan of 2.66% w/v (a and c) and 3.5% w/v (b and d).

In the current work, concentration of CHT, concentration of cross-linking agent and cross-linking time were selected for fractional factorial design based on its significant effects on drug permeation in CHT membranes (Dureja *et al* 2001; Rana *et al* 2004, 2005; Mengatto *et al* 2010). Moreover, thermal treatment was included in an experimental design for the first time. However, the effects of concentration of cross-linking agent and thermal treatment were not significant for the system under study (CHT-E2). These results contribute to demonstrate the importance of screening phase looking for active variables on the response under study in any experimental procedure.

4. Conclusions

The data presented in this work concern the study of effect of CHT membrane formulation factors on E2 flux. It was found that concentration of CHT and cross-linking time significantly affected E2 flux. The effects of concentration of cross-linking agent and thermal treatment were not significant. The statistical model developed from CCD could be used to prepare CHT membranes with specific E2 flux. For example, these membranes with specific E2 flux could have great potential application in the recycling of waste water effluents for the removal of E2 (a current contaminant) or in the pharmaceutical industry for the development of delivery systems.

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