

Asymmetric barrier model for heavy ion fusion and its relation to channel coupling

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Abstract. A new asymmetric parabolic effective fusion barrier model for heavy ion fusion is developed.

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1. Introduction

One expects that coupling effects in the mechanism of heavy ion (HI) fusion may dramatically change the shape of the barrier particularly in the region r interior to the Coulomb barrier position R_B such that there is a sharp fall of the potential in the interior region which results in an asymmetric barrier. Based on the exact transmission coefficient across an asymmetric parabolic barrier derived by Zafar Ahmed [1] and the ideas used earlier in our effective fusion barrier transmission model [2] we develop a new asymmetric parabolic effective fusion barrier model for heavy ion fusion. The expected change of shape of the barrier is represented by a variable curvature parameter ω_2 whereas the outer curvature ω_1 is kept unchanged.

2. Formulation

We explicitly use an asymmetric parabolic type barrier given by the potential

$$V(x) = \left(V_1 - \frac{1}{2} \mu \omega_1^2 x^2 \right) \theta(x) + \left(V_2 - \frac{1}{2} \mu \omega_2^2 x^2 \right) \theta(-x). \quad (1)$$

$\theta(x)$ is a step function such that $\theta(x) = 1, x > 0$ and $\theta(x) = 0, x \leq 0$. V_i and $\omega_i, i = 1, 2$ indicate the height and the curvature factors, respectively, and μ stands for the reduced mass. The potential barrier can be used to simulate the Coulomb barrier for any partial wave in the neighborhood of R_B which is taken to be at the origin in this particular expression (1). In a fusion calculation we set $V_1 = V_2 = V_B$.

By defining $\alpha_i = (V_B - E_{cm})/\hbar\omega_i$, $i = 1, 2$ and an asymmetric parameter $\eta = \sqrt{\omega_2/\omega_1}$ the transmission coefficient [1] at center of mass energy E_{cm} is given as

$$T(E_{cm}) = \frac{1}{\frac{1}{4}\sqrt{1 + e^{2\pi\alpha_1}}\sqrt{1 + e^{2\pi\alpha_2}} \left[\eta \left(\frac{f_1}{f_2} \right) + \frac{1}{\eta} \left(\frac{f_2}{f_1} \right) \right] + \frac{1}{2} [e^{\pi\alpha_1} e^{\pi\alpha_2} + 1]}, \quad (2)$$

where $f_1 = f(\alpha_1)$ and $f_2 = f(\alpha_2)$. The function $f(\alpha) = \left| \Gamma \left(\frac{1}{4} + i\frac{\alpha}{2} \right) / \Gamma \left(\frac{3}{4} + i\frac{\alpha}{2} \right) \right|$, can be approximated by $f_{\text{approx}}(\alpha) = 1/\sqrt{\gamma}(1 + 1/8\gamma)$, where $\gamma = \sqrt{(1/16) + (\alpha^2/4)}$.

In order to consider the Coulomb barriers generated by different partial waves l , we need to replace the height V_B of the effective barrier by

$$V_B^l = V_B + \frac{\hbar^2}{2\mu} \frac{l(l+1)}{R_B^2}.$$

The quantities V_B , R_B and the outer region ($r > R_B$) curvature factor ω_1 can be obtained using the following global formulae:

$$R_B = r_0 \left(A_1^{1/3} + A_2^{1/3} \right) + 2.72 \text{ fm}, \quad V_B = \frac{Z_1 Z_2 e^2}{R_B} \left(1 - \frac{a}{R_B} \right)$$

and

$$(\hbar\omega_1)^2 = \frac{Z_1 Z_2 e^2 \hbar^2}{\mu R_B^2} \left(\frac{1}{a} - \frac{2}{R_B} \right),$$

where $a = 0.63$ fm and $r_0 = 1.07$ fm, $A_j, Z_j, j = 1, 2$ denote the mass number and proton number of the two colliding nuclei, respectively. We control the inner region ($r < R_B$) curvature factor ω_2 by varying the parameter $\eta = \sqrt{\omega_2/\omega_1}$.

Using the above specifications we adopt the expression (2) to calculate transmission coefficient $T_l(E_{cm})$ for different l 's as a function of incident energy. This is then used to obtain the results for $\sigma_F^l, \sigma_F, \langle l \rangle$ and $D(E_{cm})$ given by the formulae:

$$\sigma_F^l = \frac{\pi}{k^2} (2l+1) T_l, \quad \sigma_F = \sum_{l=0}^{\infty} \sigma_F^l,$$

$$\langle l \rangle = \frac{\sum_{l=0}^{\infty} l \sigma_F^l}{\sigma_F} \quad \text{and} \quad D(E_{cm}) = \frac{d^2(E\sigma_F)}{dE^2},$$

where $k = \sqrt{(2\mu/\hbar^2)E_{cm}}$.

3. Results and discussion

In figure 1(a) and (b) (upper panel) we show by solid curve the variation of σ_F and $\langle l \rangle$, respectively, with energy for $^{40}\text{Ca} + ^{46,48,50}\text{Ti}$ systems. E_{lab} indicates energy in the laboratory frame. From these figures it is clear that fit to the experimental data is good. Values

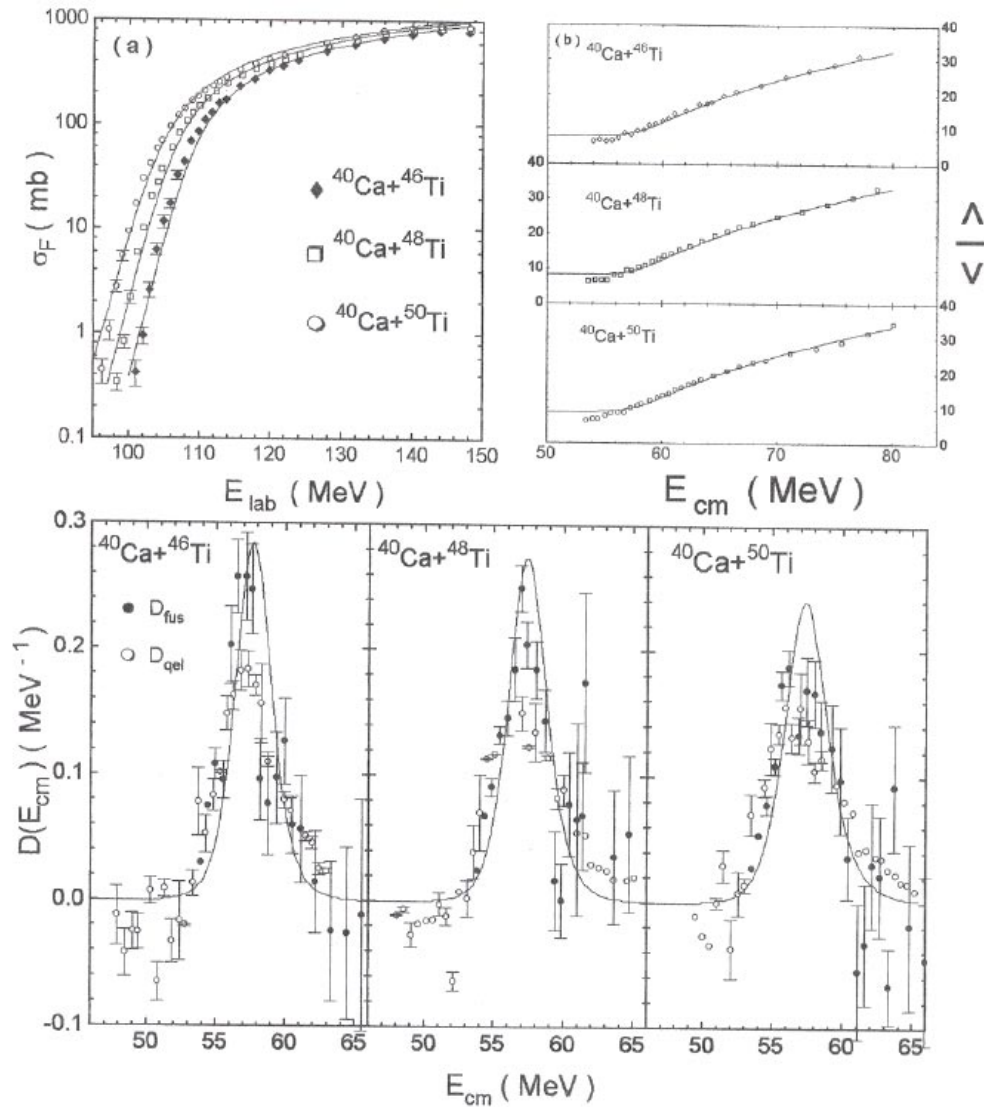


Figure 1. Upper panel shows the variation of (a) σ_F and (b) $\langle l \rangle$ with energy for $^{40}\text{Ca} + ^{46,48,50}\text{Ti}$ systems. Lower panel shows the variation of $D(E_{cm})$ with E_{cm} . Solid curves represent the results of present calculation. The experimental data are taken from ref. [4].

of V_B , R_B , $\hbar\omega_1$ and η used in the calculation for these systems are listed in table 1. In the lower panel of figure 1, we show the results for $D(E_{cm})$ obtained by using point-difference formula used in ref. [3] for the $^{40}\text{Ca} + ^{46,48,50}\text{Ti}$ systems. The fit to the experimental data in these cases is impressive. If one examines D , the D variation curve becomes broader and shorter in height for larger η as in the case of $^{40}\text{Ca} + ^{50}\text{Ti}$ system (see table 1) where more channels are involved.

Table 1. Systems and s -wave barrier radius R_B , its height V_B , curvature factor $\hbar\omega_1$ and the asymmetry parameter η .

System	R_B (fm)	V_B (MeV)	$\hbar\omega_1$ (MeV)	η
$^{40}\text{Ca} + ^{46}\text{Ti}$	10.32	57.65	4.02	1.4
$^{40}\text{Ca} + ^{48}\text{Ti}$	10.37	57.36	3.96	1.5
$^{40}\text{Ca} + ^{50}\text{Ti}$	10.39	57.76	3.91	1.8

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